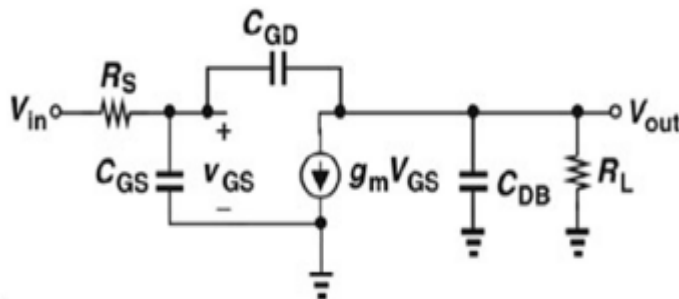
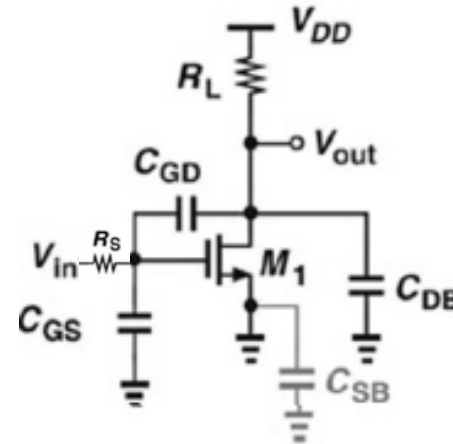
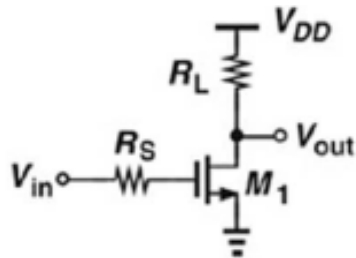


# Lect. 12: High-Frequency Response of MOS Amplifiers

(Razavi 11.1, 11.4)

- CS Amplifier

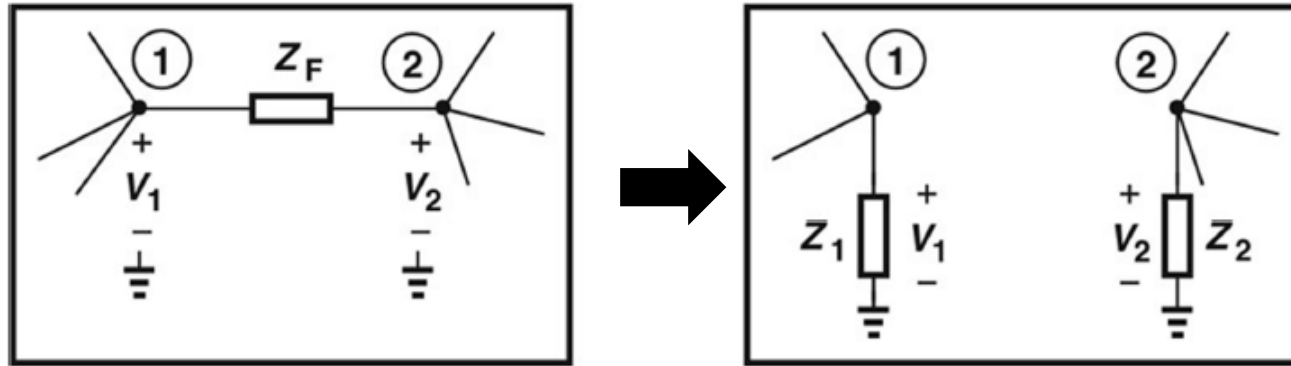


$$V_{out}(s) / V_{in}(s) = ?$$

Analysis complicated due to  $C_{GD}$  linking input to output

# Lect. 12: High-Frequency Response of MOS Amplifiers

## Miller's Theorem



$$\frac{V_1 - V_2}{Z_F} = \frac{V_1}{Z_1}$$

$$\frac{V_1 - V_2}{Z_F} = -\frac{V_2}{Z_2}$$

$$Z_1 = Z_F \frac{V_1}{V_1 - V_2}$$

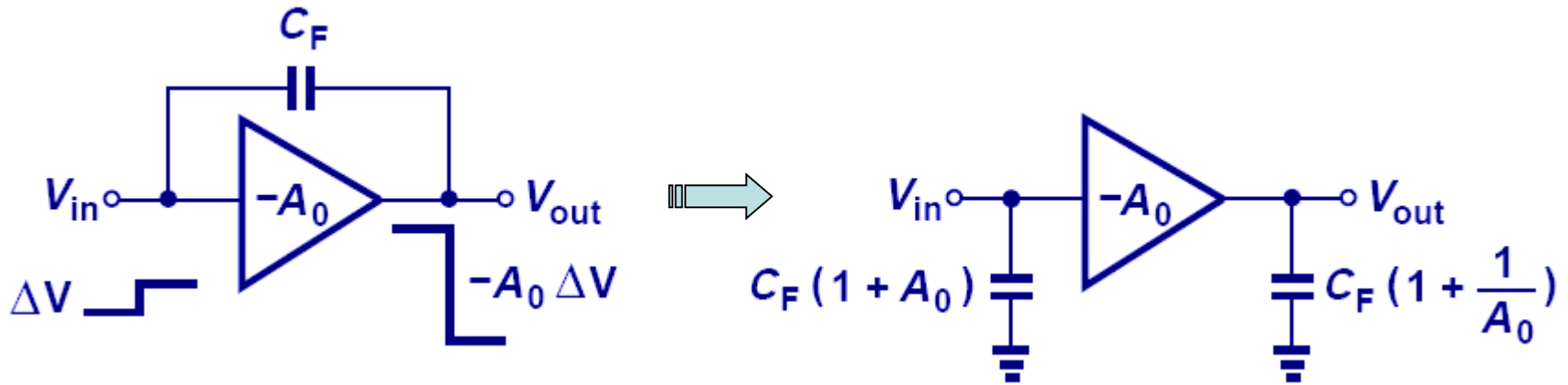
$$Z_2 = Z_F \frac{-V_2}{V_1 - V_2}$$

$$= \frac{Z_F}{1 - A_v}$$

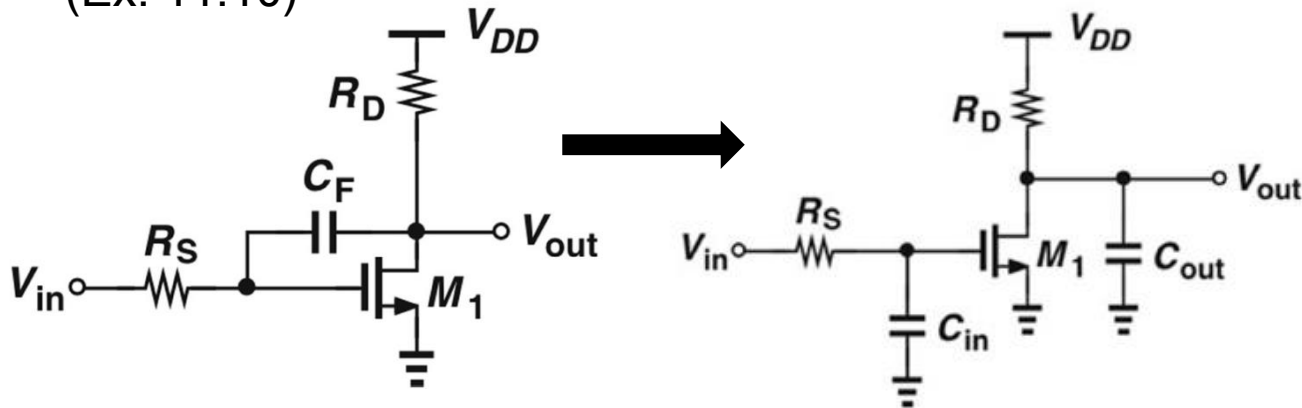
$$= \frac{Z_F}{1 - \frac{1}{A_v}}$$

# Lect. 12: High-Frequency Response of MOS Amplifiers

## Miller Multiplication



(Ex. 11.10)



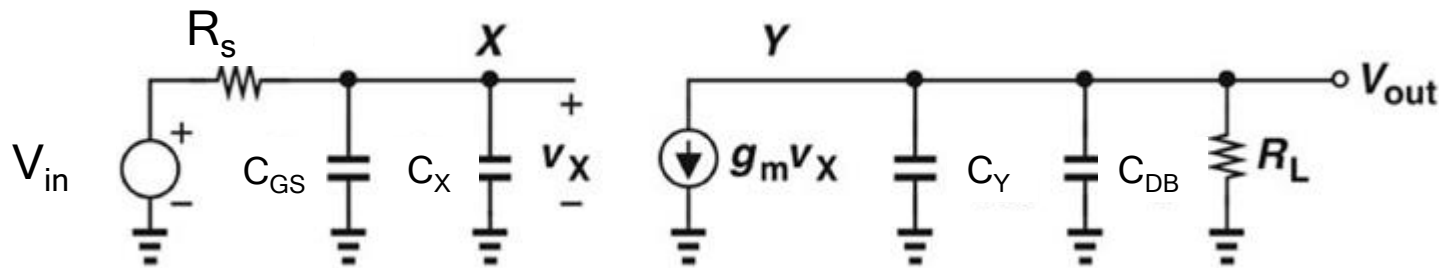
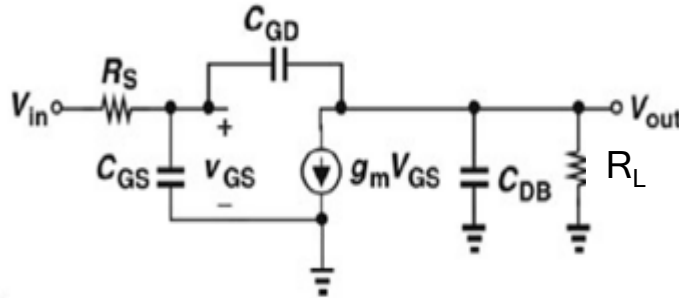
$C_{in}, C_{out}?$

$\omega_{p,in}, \omega_{p,out}?$

Approximation

# Lect. 12: High-Frequency Response of MOS Amplifiers

- CS Amplifier



$C_X, C_Y$  ?

$$C_X = C_{GD} (1 + g_m R_L)$$

$$C_Y = C_{GD} \left(1 + \frac{1}{g_m R_L}\right)$$

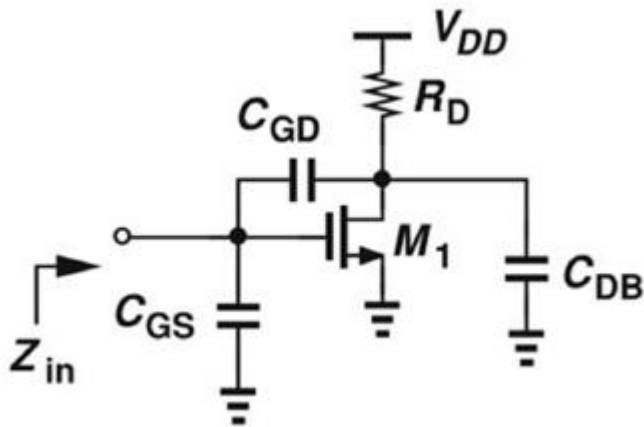
$$|\omega_{p,in}| = \frac{1}{R_S [C_{GS} + C_{GD} (1 + g_m R_L)]} \quad |\omega_{p,out}| = \frac{1}{R_L \left[ C_{DB} + C_{GD} \left(1 + \frac{1}{g_m R_L}\right) \right]}$$

Dominant capacitor?

Speed limitation by the Miller effect

# Lect. 12: High-Frequency Response of MOS Amplifiers

- Input impedance for CS Amplifier

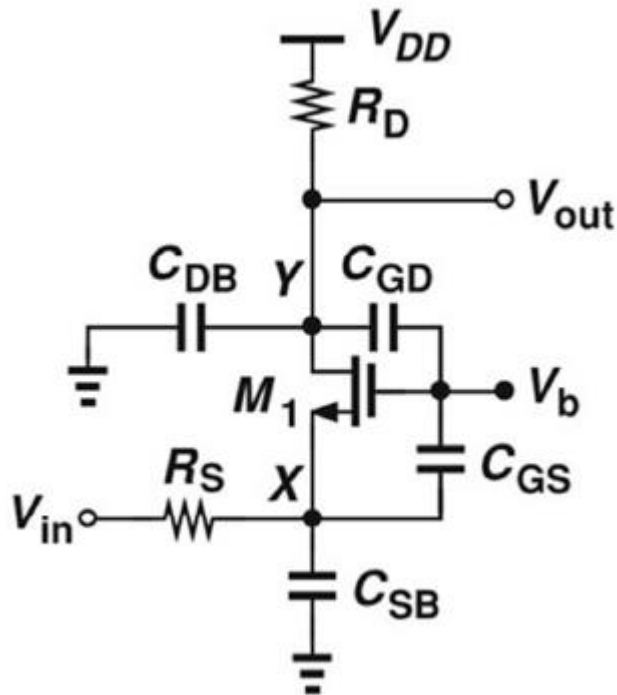


$$Z_{in} \approx \frac{1}{[C_{GS} + (1 + g_m R_D)C_{GD}]s}$$

Input impedance reduced at high freq. due to Miller effect

# Lect. 12: High-Frequency Response of MOS Amplifiers

- CG Amplifier



$$|\omega_{p,X}| = \frac{1}{\left(R_S \parallel \frac{1}{g_m}\right)(C_{GS} + C_{SB})}$$

$$|\omega_{p,Y}| = \frac{1}{R_D(C_{DB} + C_{GD})}$$

No speed limitation by the Miller effect

# Lect. 12: High-Frequency Response of MOS Amplifiers

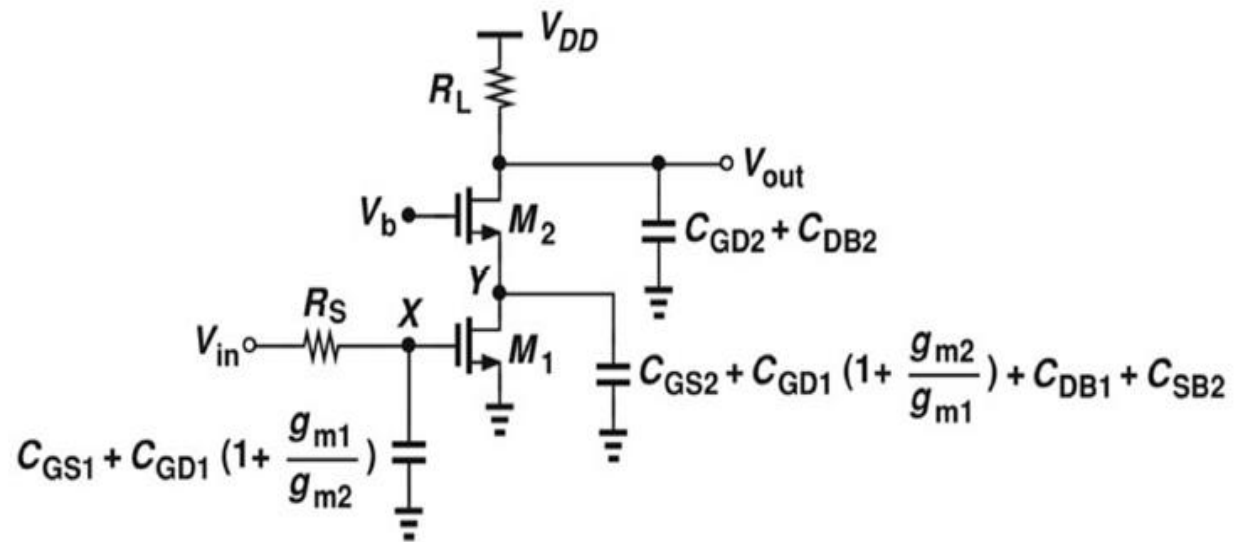
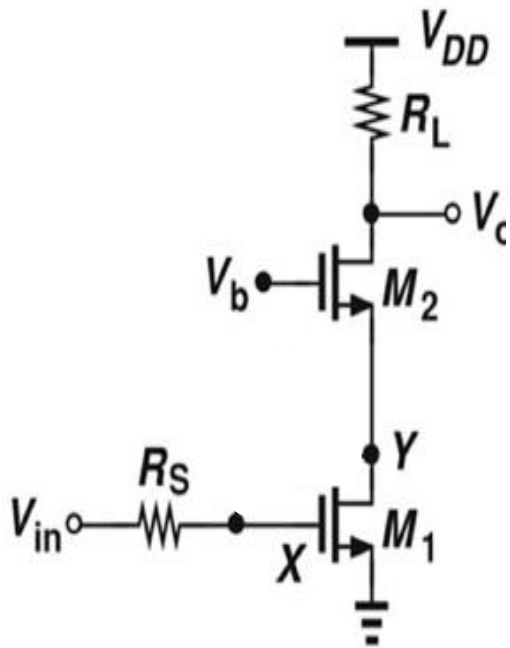
- Cascode Amplifier

- CS and then CG

- Add capacitors for each transistor

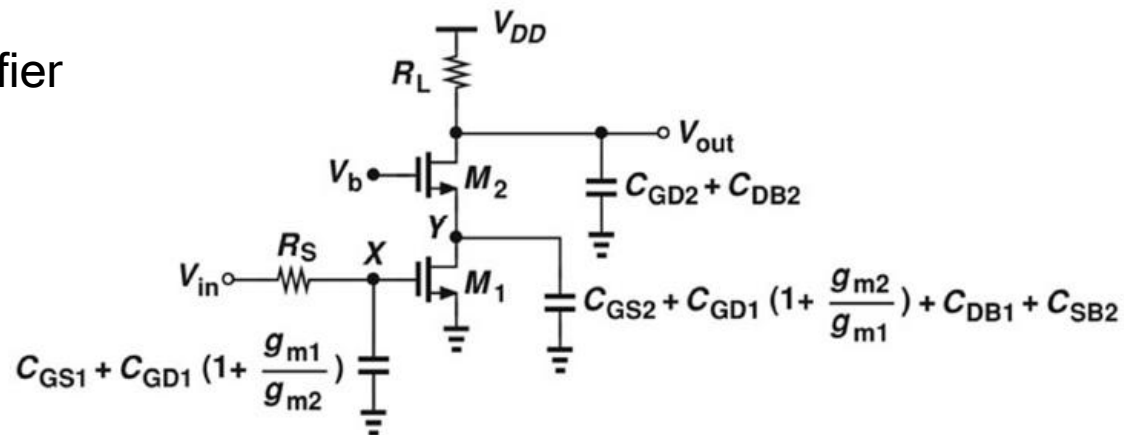
- Simplify

- Replace  $C_{GD1}$  with  $C_{in,1}$  and  $C_{out,1}$



# Lect. 12: High-Frequency Response of MOS Amplifiers

## - Cascode Amplifier



$$|\omega_{p,X}| = \frac{1}{R_S [C_{GS1} + \left(1 + \frac{g_{m1}}{g_{m2}}\right) C_{GD1}]}$$

$$|\omega_{p,Y}| = \frac{1}{\frac{1}{g_{m2}} [C_{DB1} + C_{GS2} + \left(1 + \frac{g_{m2}}{g_{m1}}\right) C_{GD1} + C_{SB2}]}$$

$$|\omega_{p,out}| = \frac{1}{R_L (C_{DB2} + C_{GD2})}$$

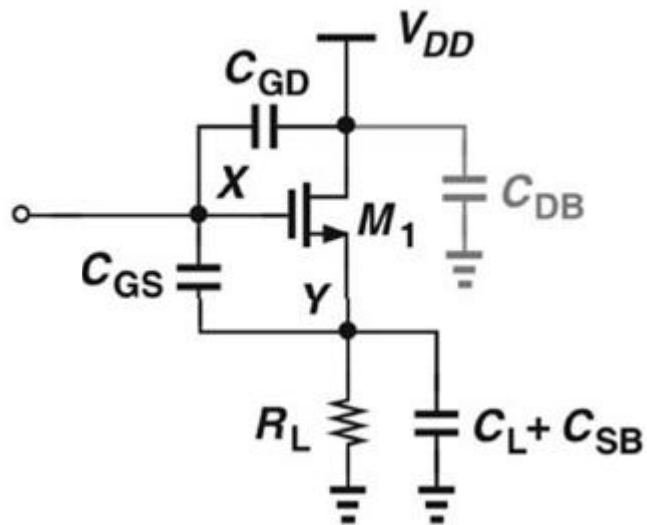
- Does this suffer from Miller effect?

- Cascode amp provides larger gain-bandwidth product than CS



# Lect. 12: High-Frequency Response of MOS Amplifiers

- Source Follower



$$C_{in} = C_{GD} + C_{GS}(1 - AV)$$

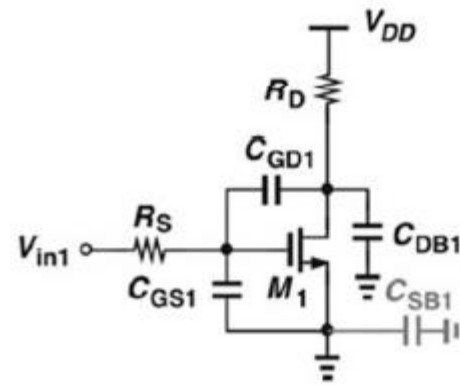
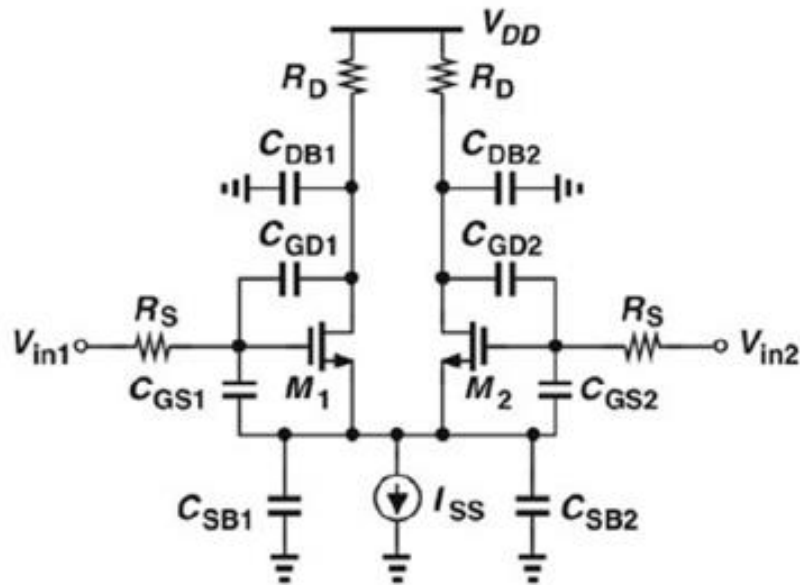
$$A_v = \frac{R_L}{R_L + \frac{1}{g_m}}$$

$$Z_{in} = \frac{1}{\left( C_{GD} + C_{GS} \frac{1}{1 + g_m R_L} \right) s}$$

Does this suffer from Miller effect?

# Lect. 12: High-Frequency Response of MOS Amplifiers

## - Differential Amplifier



→ CS amplifier

# Lect. 12: High-Frequency Response of MOS Amplifiers

## Homework

Assuming  $\lambda > 0$  and using Miller's theorem, determine the input and output poles of the stages

