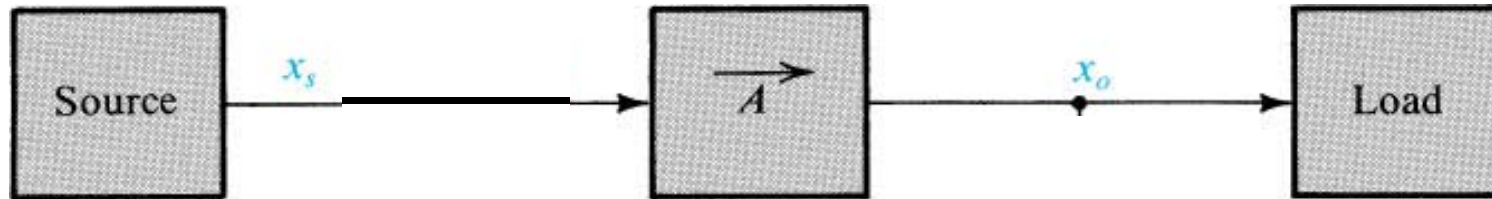


Lect. 13: Feedback

(12.1, 12.2 in Razavi)

Feedback

Amplifier



$$x_o = Ax_s$$

$$x_f = \beta x_o \quad (\text{Assume } \beta \text{ is positive})$$

$$x_i = x_s - x_f = x_s - \beta x_o$$

$$x_o = Ax_i = A(x_s - \beta x_o)$$

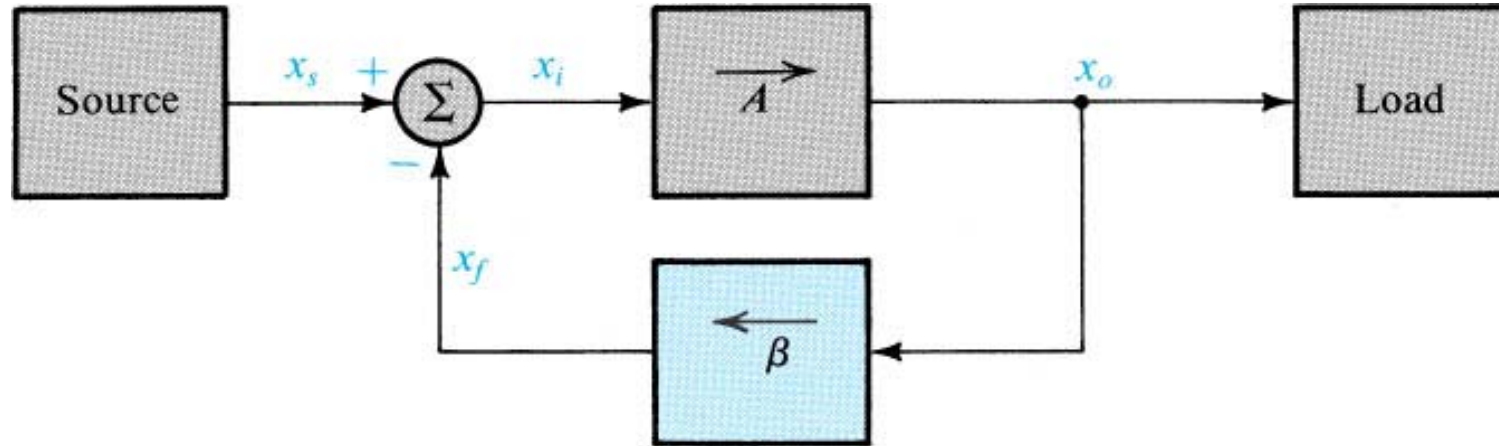
$$x_o(1 + A\beta) = Ax_s$$

$$\therefore A_f = \frac{x_o}{x_s} = \frac{A}{1 + A\beta}$$

(Closed loop gain)

$A\beta$ (loop gain)

Lect. 13: Feedback



$$A_f = \frac{x_o}{x_s} = \frac{A}{1 + A\beta} \sim \frac{1}{\beta} \quad (\text{If } A\beta \gg 1)$$

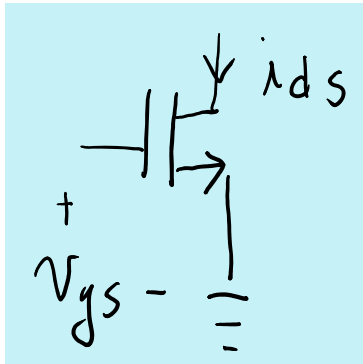
What good is it?

A_f is not influenced by changes in A

→ Gain Desensitivity

Lect. 13: Feedback

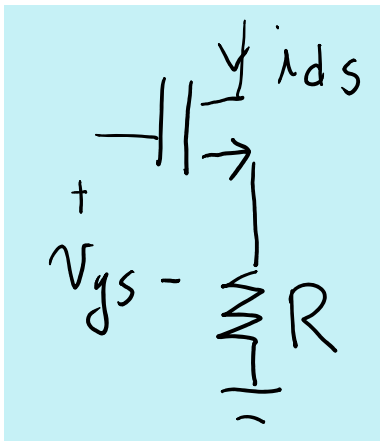
Example: Consider CS transconductance amplifier



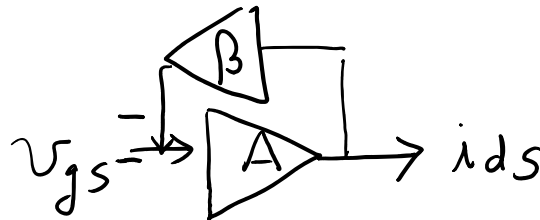
$$G_m = i_{ds}/v_{gs} = g_m = \sqrt{2\mu_n C_{ox} \cdot \frac{W}{L} \cdot I_D}$$

If g_m cannot be controlled very well
(bias conditions, process variations, temp., etc)

→ Amplifier performance is not predictable



Feedback: source resistance



$$A_f = \frac{A}{1 + A\beta}$$

$$G_m = \frac{i_{ds}}{v_{gs}} = \frac{g_m}{1 + g_m R} \sim \frac{1}{R}$$

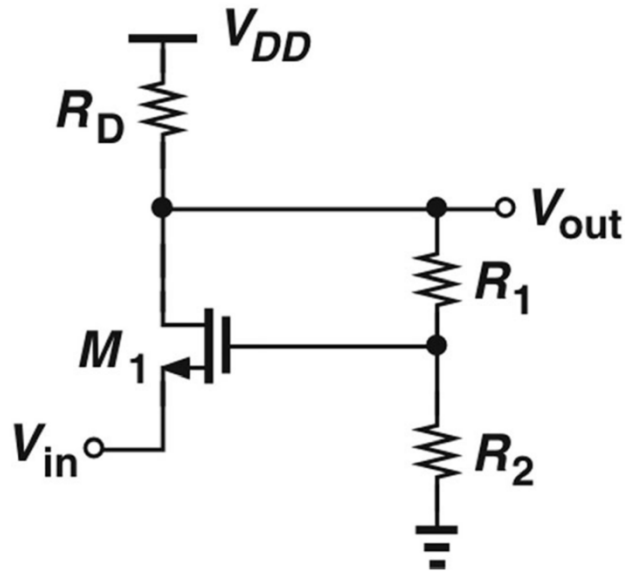
G_m is controlled by R !

$$A = g_m \quad \beta = R$$

(Assuming R is well controlled →
design using discrete components)

Lect. 13: Feedback

Example 12.7 : CG with feedback
(Assume $R_1 + R_2 \gg R_D$, $\lambda = 0$)



$$V_{\text{out}} / V_{\text{in}} = ?$$

$$A_f = \frac{A}{1 + A\beta}$$

$$A \sim g_m R_D$$

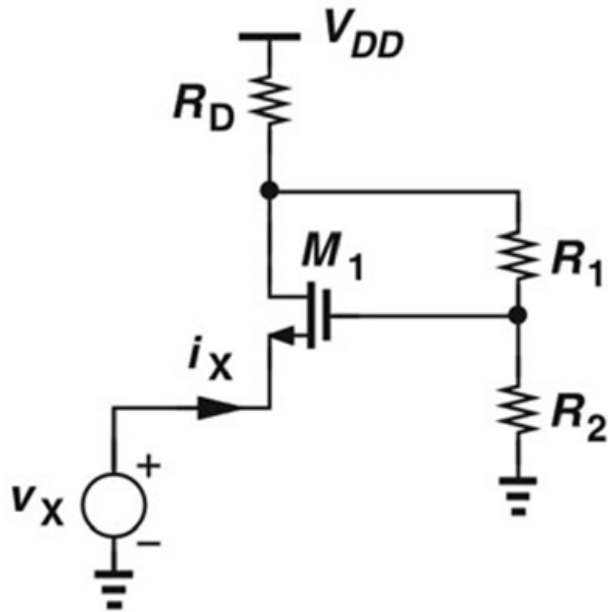
$$\beta = \frac{R_2}{R_1 + R_2}$$

$$V_{\text{out}} / V_{\text{in}} = \frac{g_m R_D}{1 + \frac{R_2}{R_1 + R_2} g_m R_D}$$

Lect. 13: Feedback

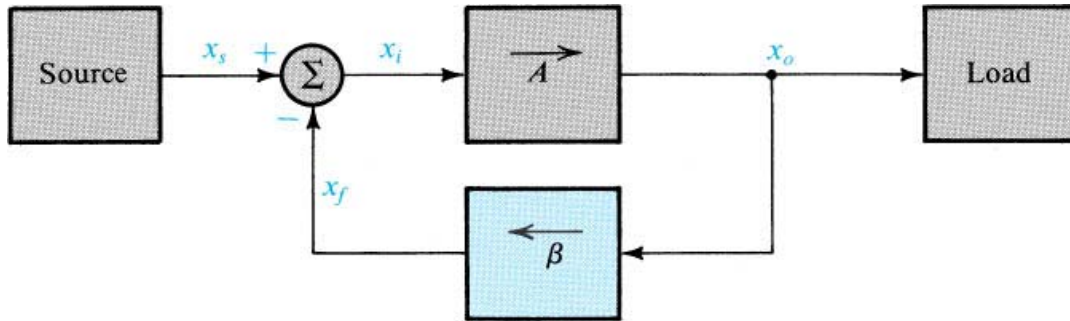
Example 12.7 : CG with feedback
(Assume $R_1 + R_2 \gg R_D$, $\lambda = 0$)

$$R_{in} = ?$$



Lect. 13: Feedback

Frequency Response of Feedback System



Assume $A(s) = \frac{A_M}{1 + s/\omega_H}$

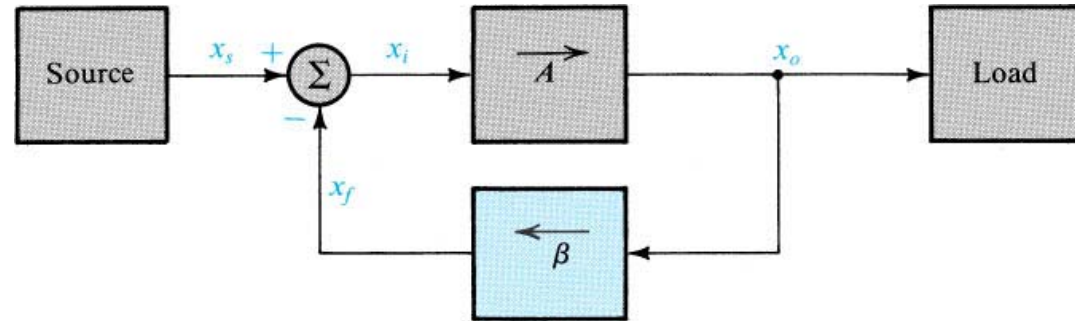
Then $A_f(s) = \frac{A(s)}{1 + \beta A(s)}$

$$A_f(s) = \frac{\frac{A_M}{1 + s/\omega_H}}{1 + \beta \frac{A_M}{1 + s/\omega_H}} = \frac{A_M}{1 + A_M\beta + s/\omega_H} = \frac{A_M / (1 + A_M\beta)}{1 + s/\omega_H (1 + A_M\beta)}$$

$\omega_{Hf} = \omega_H (1 + A_M\beta)$ Bandwidth extension!

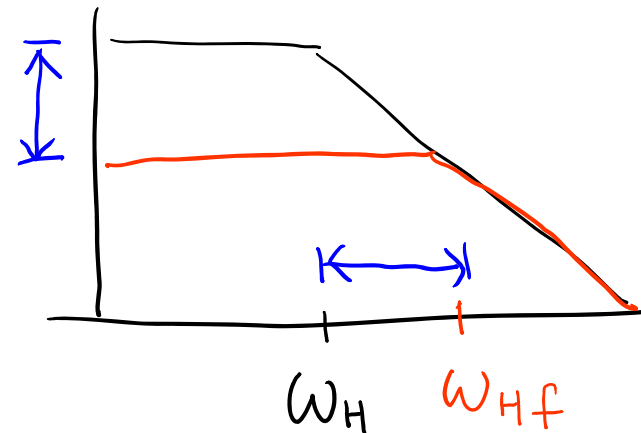
Reduction in LF gain

Lect. 13: Feedback



$$A(s) = \frac{A_M}{1 + s / \omega_H}$$

$$A_f(s) = \frac{A_M / (1 + A_M \beta)}{1 + s / \omega_H (1 + A_M \beta)}$$



Lect. 13: Feedback

Is feedback always possible? → Stability of feedback system

$$A_f(s) = \frac{A(s)}{1 + \beta A(s)}$$

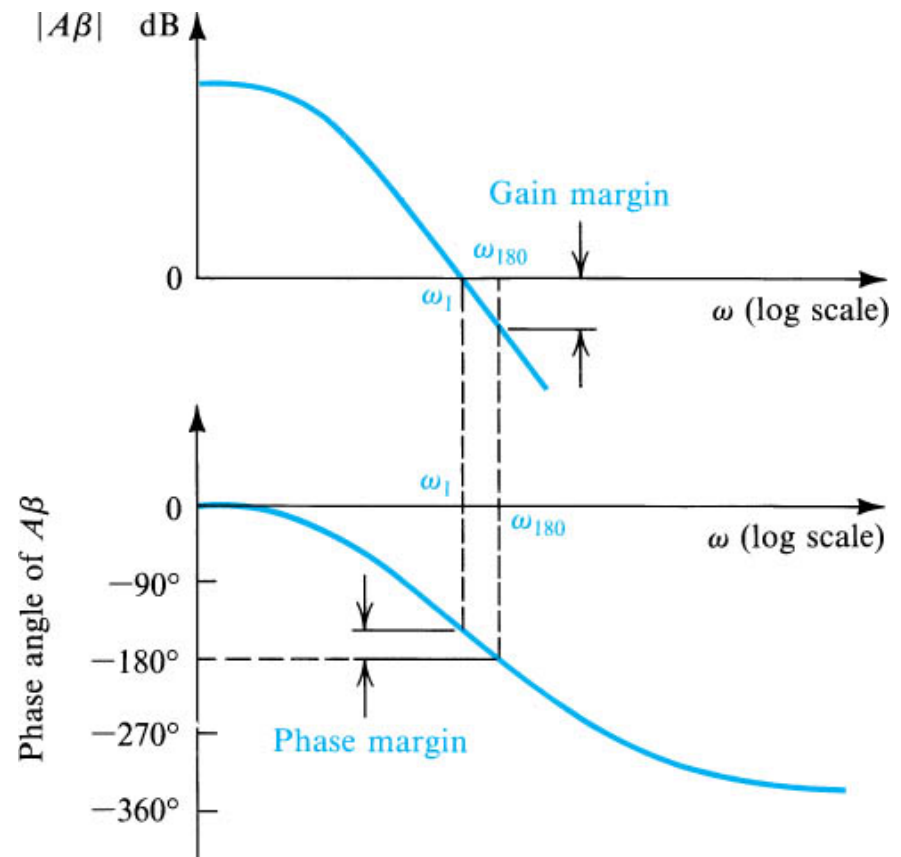
If $\beta A(s) = -1$, system becomes unstable !

For stable feedback system design,

Phase $[\beta A(s)] > -180$ deg when $|\beta A(s)| = 1$

→ The larger β is, less phase margin

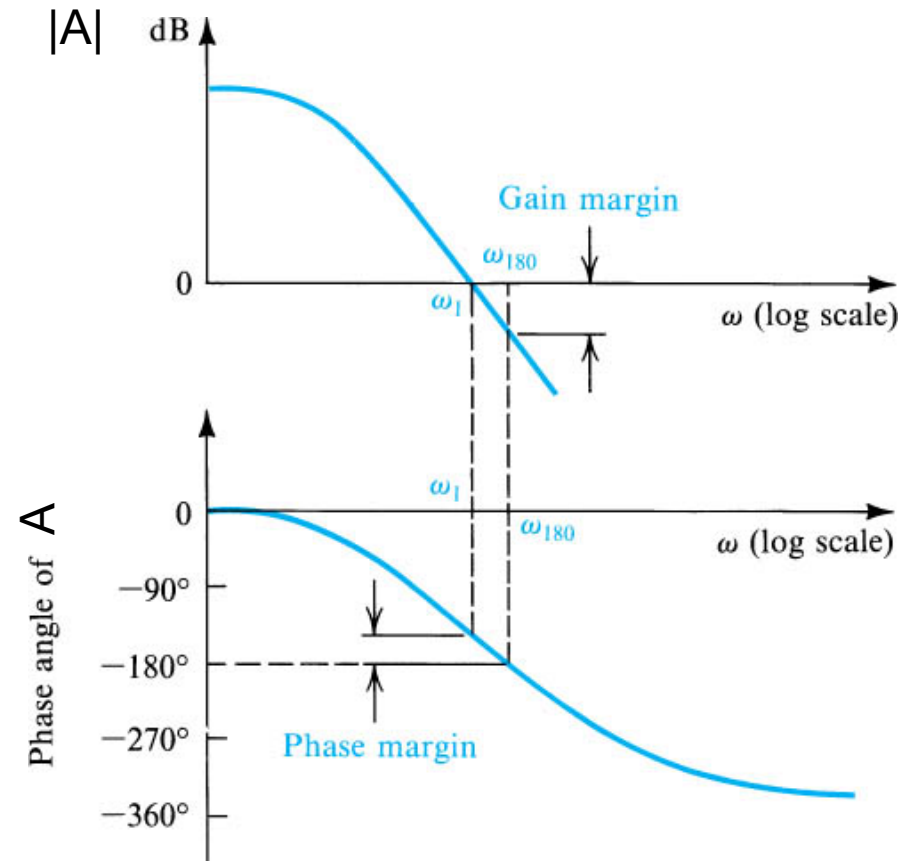
How should we design our amplifier for feedback applications?



Lect. 13: Feedback

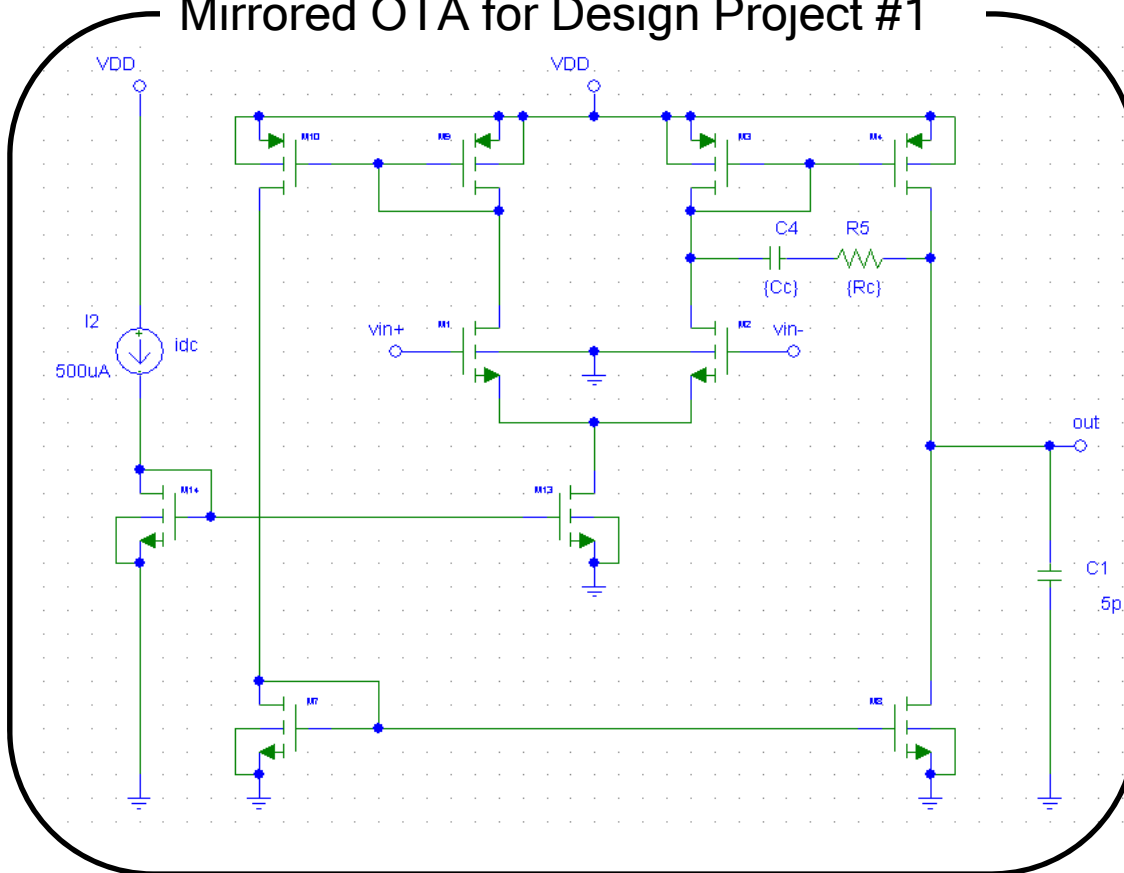
When designing amplifiers
for feedback applications
(Example, OTA for our design project)

→ Provide sufficient phase margin



Lect. 13: Feedback

Mirrored OTA for Design Project #1



- Mirrored OTA Specifications

| Parameter | Value |
|-------------------|----------|
| A_V | > 56dB |
| Bandwidth | > 60KHz |
| Phase Margin | > 65° |
| V_{p-p} | > 1.5V |
| Slew Rate | > 13MV/s |
| CMRR | > 85dB |
| Power Consumption | < 2.5mW |