

Lect. 20: Two-Integrator-Loop Biquad

(Razavi 14.4.2)

One circuit configuration for several different second-order filters?

→ Two-integrator-loop biquad

Consider high-pass filter

$$\frac{V_{hp}}{V_i} = \frac{Ks^2}{s^2 + s(\omega_0/Q) + \omega_0^2}$$

$$V_{hp}s^2 + V_{hp}s(\omega_0/Q) + V_{hp}\omega_0^2 = KV_i s^2$$

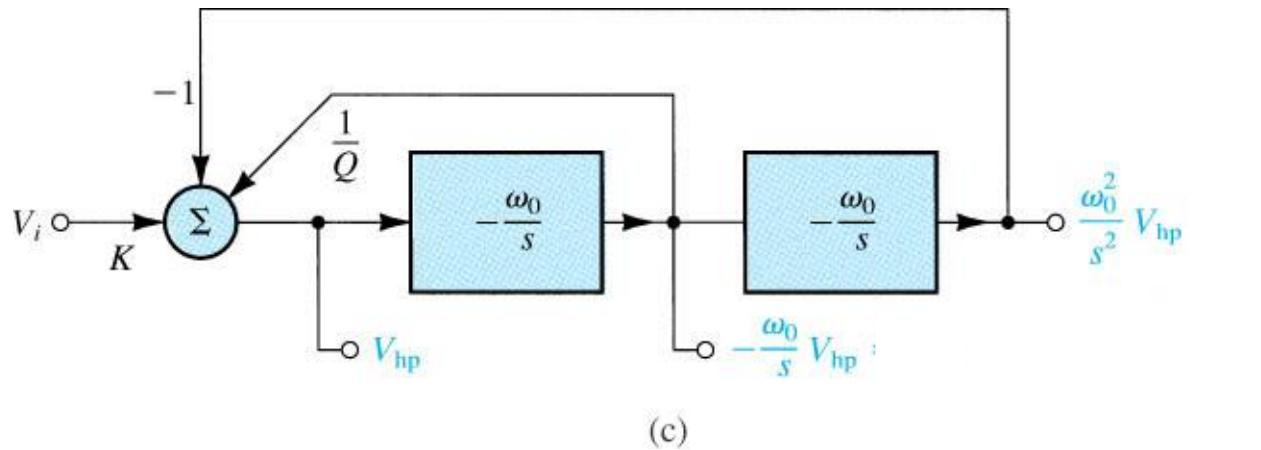
$$V_{hp} + \frac{1}{Q} \left(\frac{\omega_0}{s} V_{hp} \right) + \left(\frac{\omega_0^2}{s^2} V_{hp} \right) = KV_i$$

$$V_{hp} = KV_i - \frac{1}{Q} \frac{\omega_0}{s} V_{hp} - \frac{\omega_0^2}{s^2} V_{hp}$$

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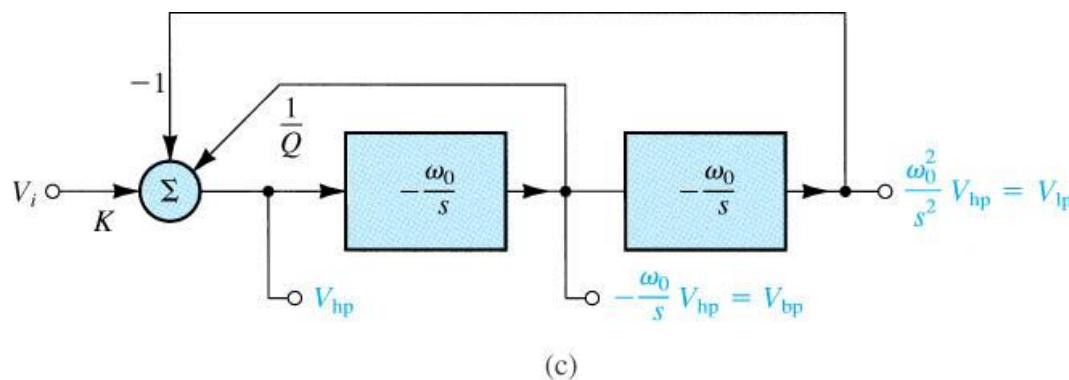
$$V_{hp} = KV_i - \frac{1}{Q} \frac{\omega_0}{s} V_{hp} - \frac{\omega_0^2}{s^2} V_{hp}$$

Express the above equation using a block diagram

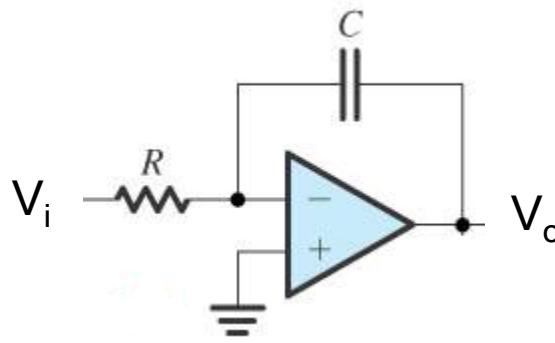
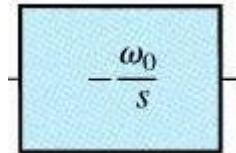


Biquad → Universal Active Filter

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How to implement biquad?



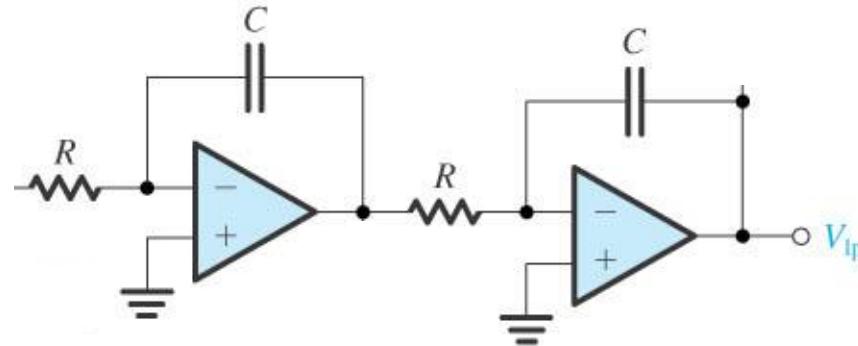
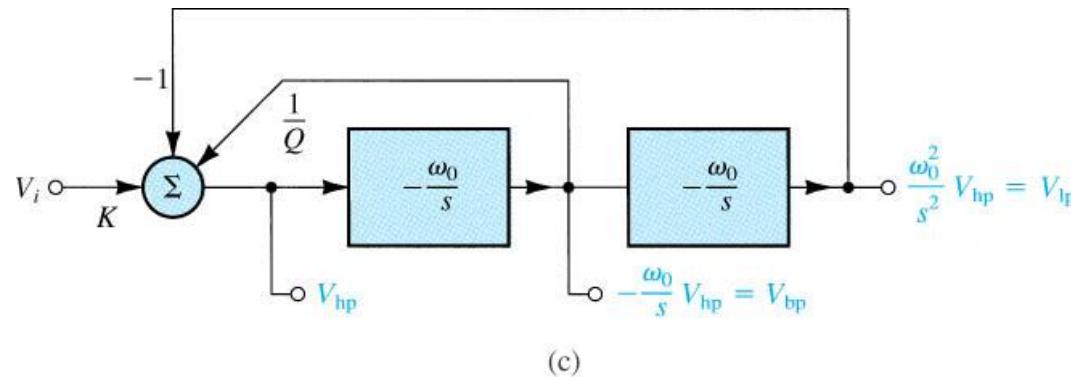
$$V_o = -\frac{V_i}{R} \cdot \frac{1}{sC}$$

$$\frac{V_o}{V_i} = -\frac{1}{RCs} = -\frac{\omega_0}{s}$$

$$\omega_0 = \frac{1}{RC}$$

(Ignoring the op-amp offset)

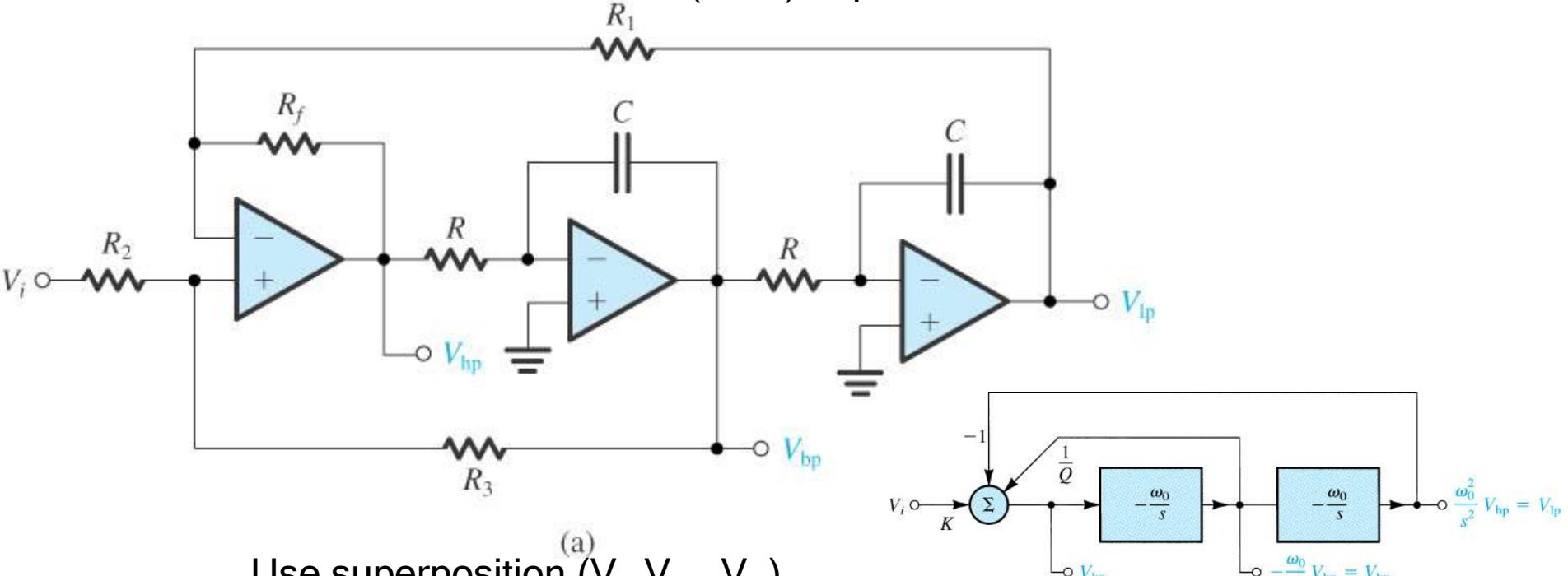
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(a)

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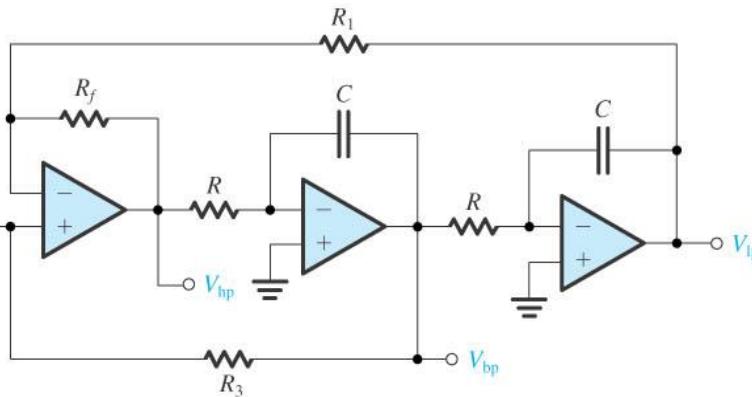
Kerwin-Huelsman-Newcomb (KHN) biquad



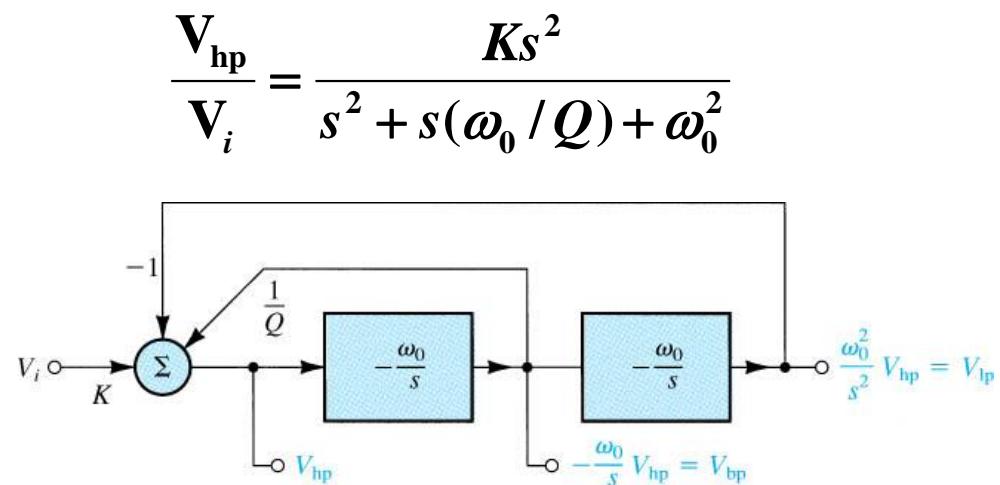
→ Weighted sum of V_i , V_{bp} , V_{lp}

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KHN



$$V_{hp} = \frac{R_3}{R_2 + R_3} \left(\frac{R_1 + R_f}{R_1} \right) V_i + \frac{R_2}{R_2 + R_3} \left(1 + \frac{R_f}{R_1} \right) V_{bp} - \frac{R_f}{R_1} V_{lp}$$



$$(c) \quad V_{hp} = KV_i + \frac{1}{Q} V_{bp} - V_{lp}$$

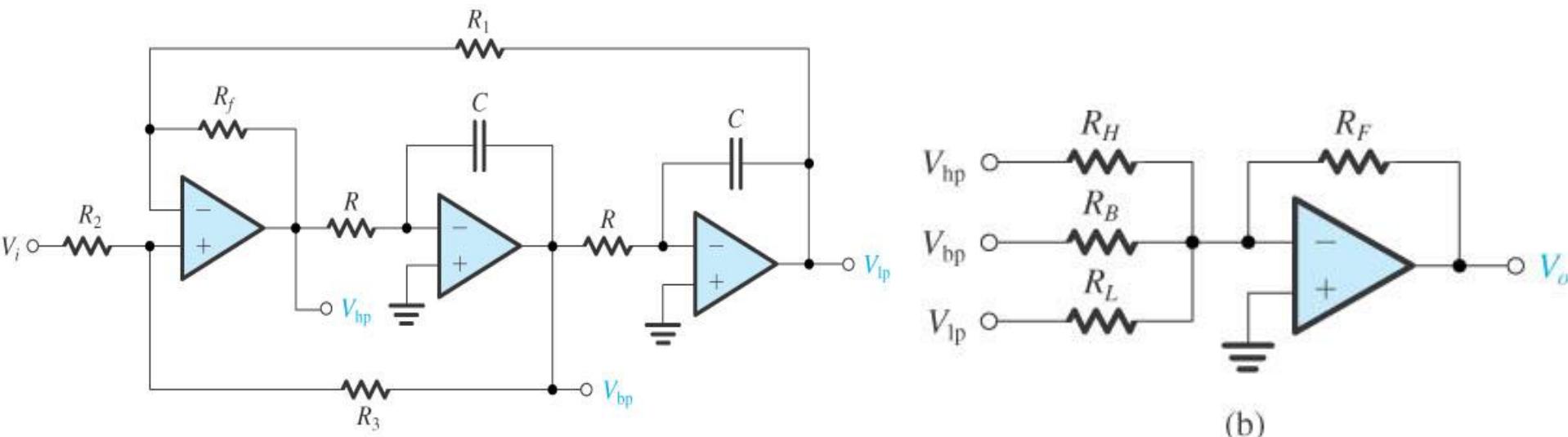
$$\therefore R_f/R_1 = 1 \quad \frac{2R_2}{R_2 + R_3} = \frac{1}{Q} \quad \therefore Q = \frac{R_2 + R_3}{2R_2} \quad K = \frac{2R_3}{R_2 + R_3} \quad \omega_0 = ?$$

All of HF, LP and BP characteristics can be obtained!

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How about All-Pass Filter?

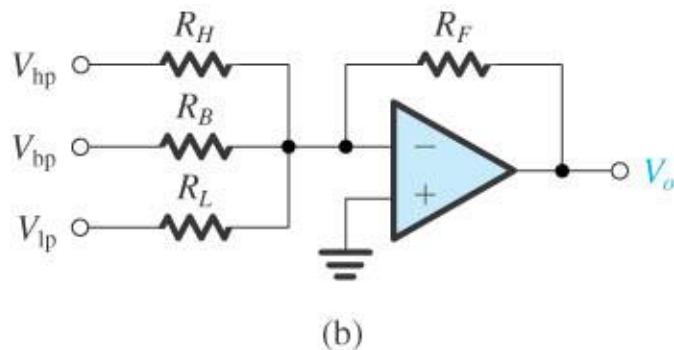
Can be realized by linear combination of V_{hp} , V_{bp} , V_{lp}



KHN

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All-Pass Filters



$$\mathbf{V}_o = - \left(\frac{\mathbf{R}_F}{\mathbf{R}_H} \mathbf{V}_{hp} + \frac{\mathbf{R}_F}{\mathbf{R}_B} \mathbf{V}_{bp} + \frac{\mathbf{R}_F}{\mathbf{R}_L} \mathbf{V}_{lp} \right)$$

$$\mathbf{V}_{hp} = \frac{Ks^2}{s^2 + s(\omega_0/Q) + \omega_0^2} \mathbf{V}_i$$

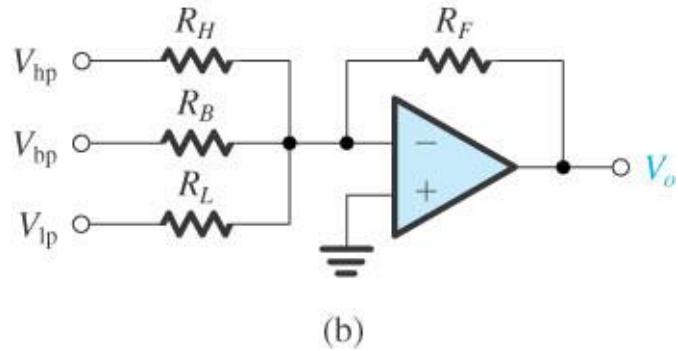
$$\mathbf{V}_{bp} = \left(-\frac{\omega_0}{s} \right) \mathbf{V}_{hp} = \frac{-K\omega_0 s}{s^2 + s(\omega_0/Q) + \omega_0^2} \mathbf{V}_i$$

$$\mathbf{V}_{lp} = \left(\frac{\omega_0^2}{s^2} \right) \mathbf{V}_{hp} = \frac{K\omega_0^2}{s^2 + s(\omega_0/Q) + \omega_0^2} \mathbf{V}_i$$

$$\frac{\mathbf{V}_o}{\mathbf{V}_i} = - \frac{(\mathbf{R}_F / \mathbf{R}_H) K s^2 - (\mathbf{R}_F / \mathbf{R}_B) K \omega_0 s + (\mathbf{R}_F / \mathbf{R}_L) K \omega_0^2}{s^2 + s(\omega_0/Q) + \omega_0^2}$$

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How about All-Pass Filters?



$$\frac{V_o}{V_i} = -K \frac{(R_F / R_H)s^2 - (R_F / R_B)\omega_0 s + (R_F / R_L)\omega_0^2}{s^2 + s(\omega_0 / Q) + \omega_0^2}$$

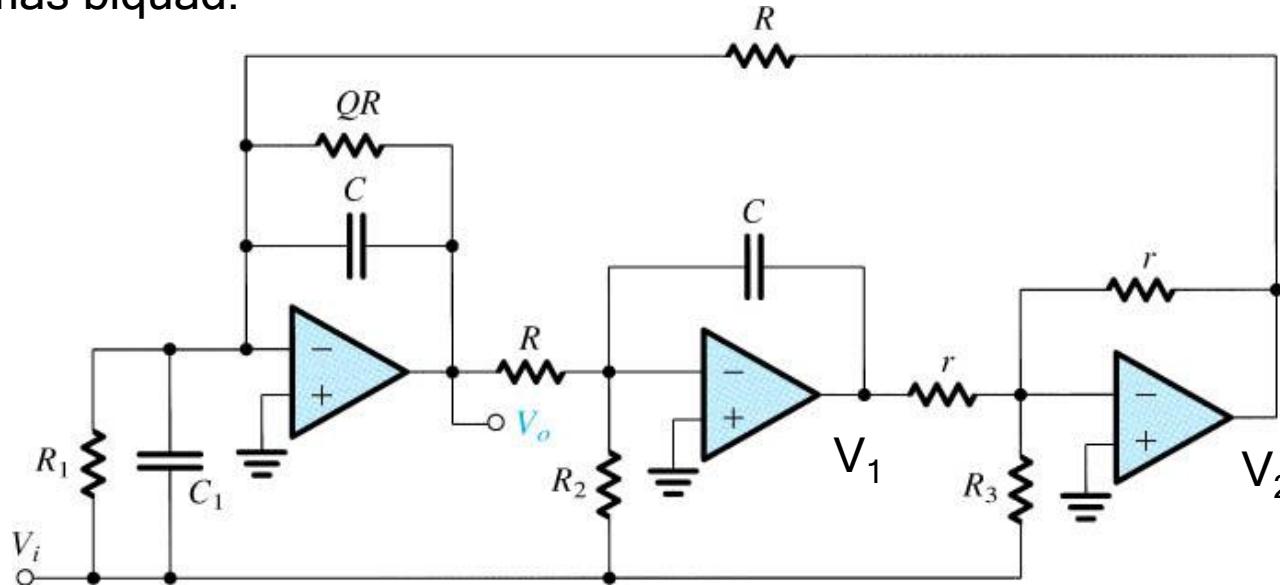
(b)

All-Pass Filter $T(s) = a_2 \frac{s^2 - s \frac{\omega_0}{Q} + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$ $\frac{R_F}{R_H} = 1, \quad \frac{R_F}{R_B} = \frac{1}{Q}, \quad \frac{R_F}{R_L} = 1$

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There are several Biquads

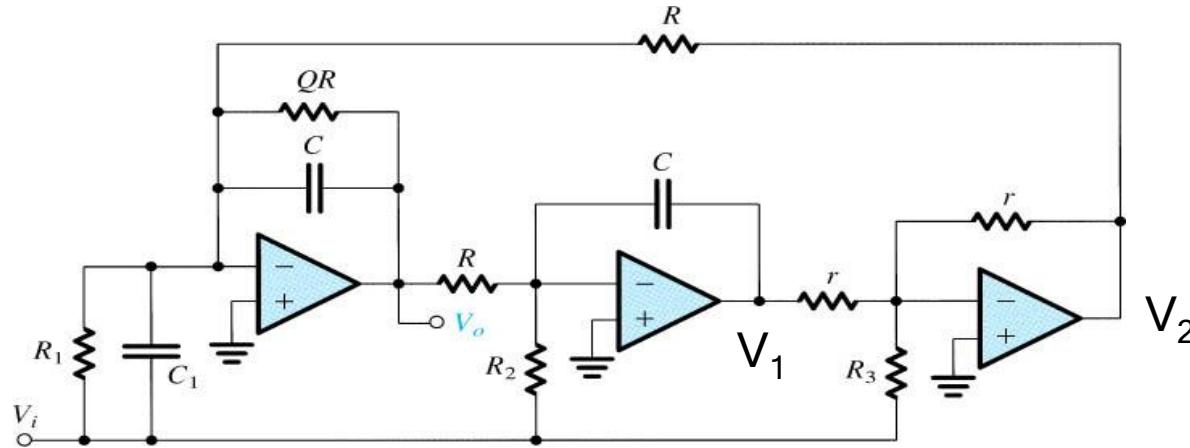
Tow-Thomas biquad:



$$V_o = - \left(\frac{V_i}{R_1 // \frac{1}{sC_1}} + \frac{V_2}{R} \right) (QR // \frac{1}{sC}) \quad V_1 = - \left(\frac{V_o}{R} + \frac{V_i}{R_2} \right) \frac{1}{sC} \quad V_2 = - \left(\frac{V_i}{R_3} + \frac{V_1}{r} \right) r$$

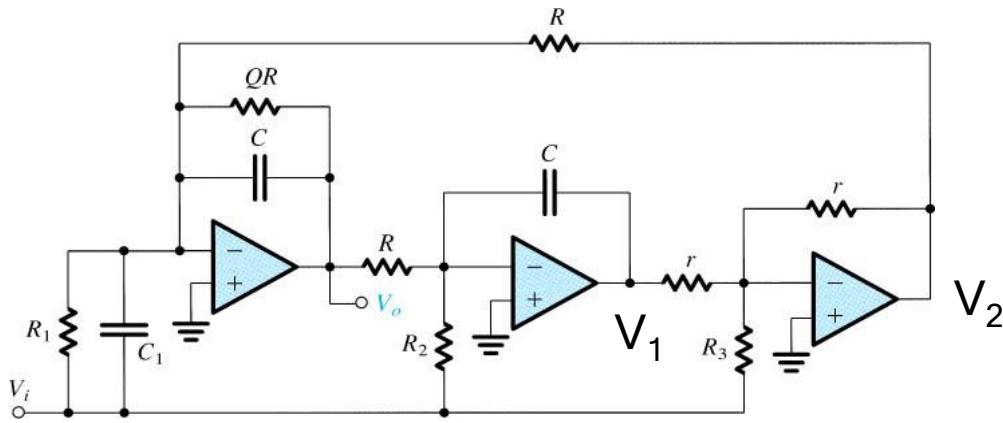
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Tow-Thomas biquad



$$\frac{V_o}{V_i} = - \frac{s^2 \left(\frac{C_1}{C} \right) + s \frac{1}{C} \left(\frac{1}{R_1} - \frac{r}{RR_3} \right) + \frac{1}{C^2 RR_2}}{s^2 + s \frac{1}{QCR} + \frac{1}{C^2 R^2}}$$
$$\omega_0 = \frac{1}{CR}$$

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$$\frac{V_o}{V_i} = - \frac{s^2 \left(\frac{C_1}{C} \right) + s \frac{1}{C} \left(\frac{1}{R_1} - \frac{r}{RR_3} \right) + \frac{1}{C^2 RR_2}}{s^2 + s \frac{1}{QCR} + \frac{1}{C^2 R^2}}$$

For LP $T(s) = \frac{a_0}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$

$$C_1 = 0 \quad R_1 = \infty, \quad R_3 = \infty$$

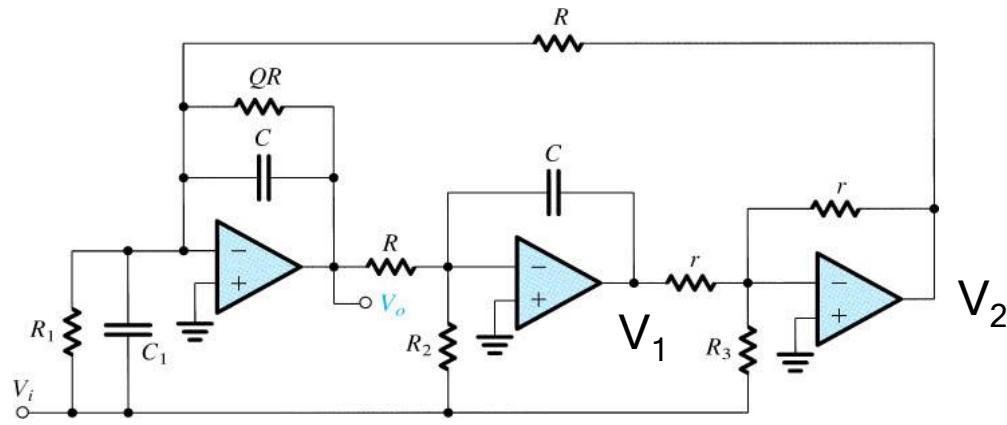
DC Gain: $\frac{R}{R_2}$

For HP $T(s) = \frac{a_2 s^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$

$$R_1 = \infty, \quad R_2 = \infty, \quad R_3 = \infty$$

HF Gain: $\frac{C_1}{C}$

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For BP

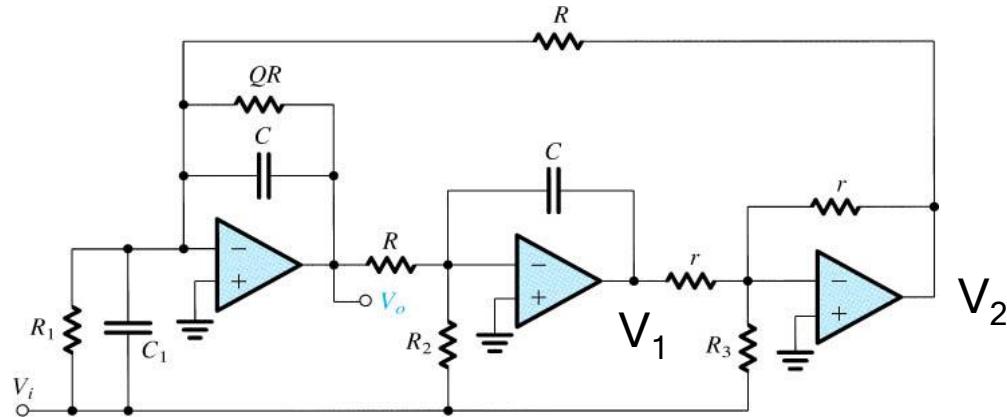
$$T(s) = \frac{a_1 s}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$

$$C_1 = 0 \quad R_2 = \infty$$

$$a_1 = \frac{1}{C} \left(\frac{1}{R_1} - \frac{r}{RR_3} \right)$$

$$\frac{V_o}{V_i} = - \frac{s^2 \left(\frac{C_1}{C} \right) + s \frac{1}{C} \left(\frac{1}{R_1} - \frac{r}{RR_3} \right) + \frac{1}{C^2 RR_2}}{s^2 + s \frac{1}{QCR} + \frac{1}{C^2 R^2}}$$

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For AP

$$T(s) = a_2 \frac{s^2 - s \frac{\omega_0}{Q} + \omega_0^2}{s^2 + s \frac{\omega_0}{Q} + \omega_0^2}$$

$$C_1 = C$$

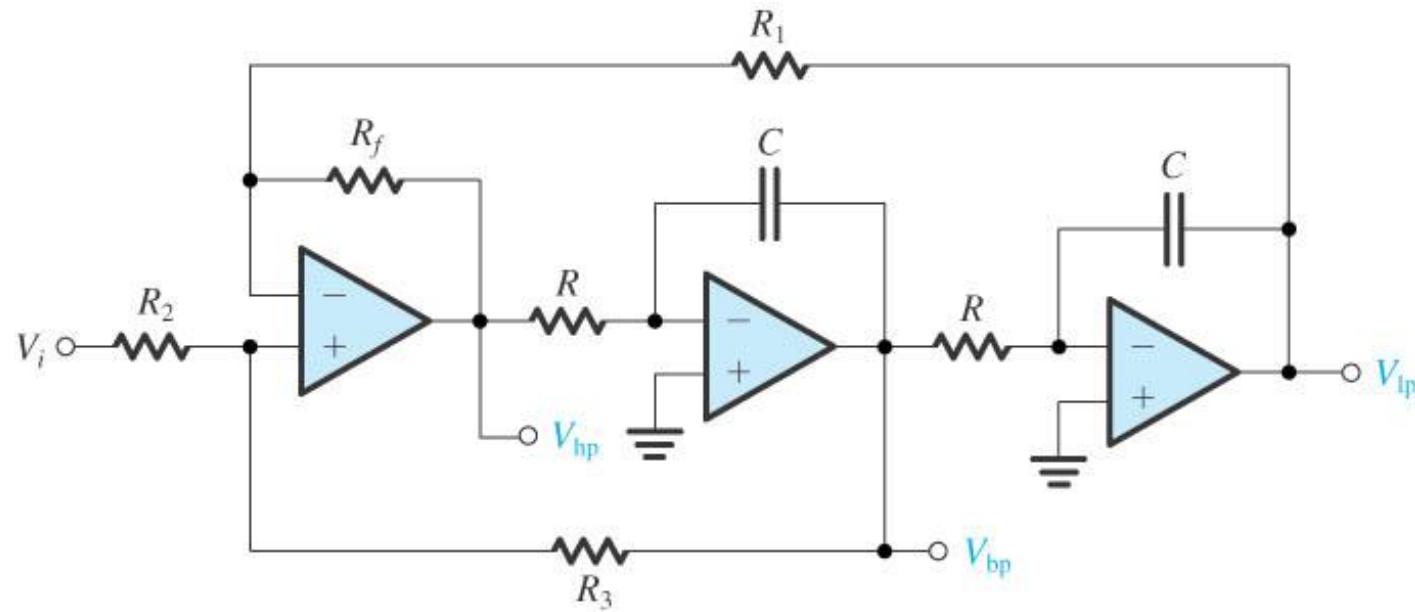
$$R_1 = \infty \quad R_3 = Qr$$

$$R_2 = R$$

$$\frac{V_o}{V_i} = - \frac{s^2 \left(\frac{C_1}{C} \right) + s \frac{1}{C} \left(\frac{1}{R_1} - \frac{r}{RR_3} \right) + \frac{1}{C^2 RR_2}}{s^2 + s \frac{1}{QCR} + \frac{1}{C^2 R^2}}$$

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Homework(1) Determine $V_{hp}(s)/V_i(s)$, $V_{bp}(s)/V_i(s)$, $V_{lp}(s)/V_i(s)$



(a)

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Homework(2): Determine $V_o(s)/V_i(s)$

