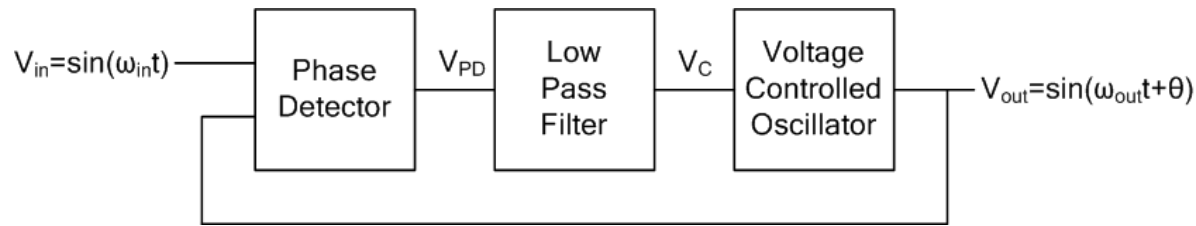


# Lect. 27: Charge-Pump PLL



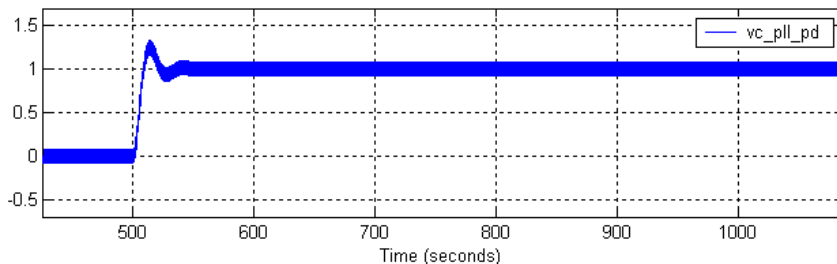
$$H(s) = \frac{K_{PD} K_{VCO} \omega_p}{s^2 + \omega_p s + K_{PD} K_{VCO} \omega_p}$$

This type of PLL has very narrow locking range

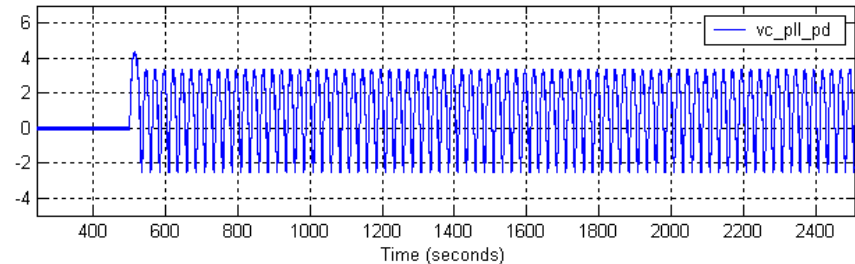
Step response simulation:

$$f_{in} = 1\text{Hz}, K_{PD} = 5\text{V} / \text{rad}, K_{VCO} = 2\pi \times 0.01\text{rad} / \text{s} / \text{V}, \text{ and } f_p = 0.032\text{Hz}$$

$$\Delta f_{in} = 0.01\text{Hz}$$



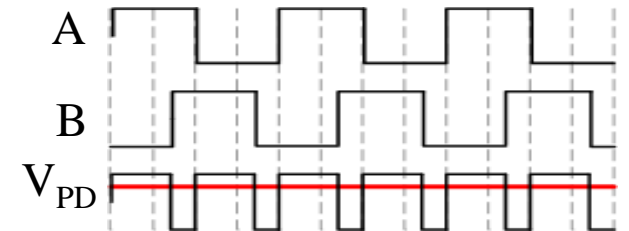
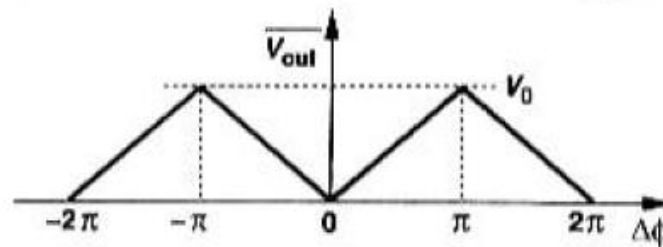
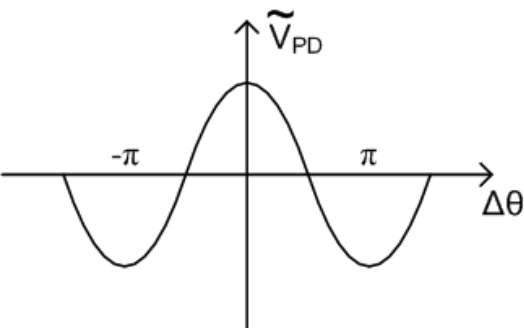
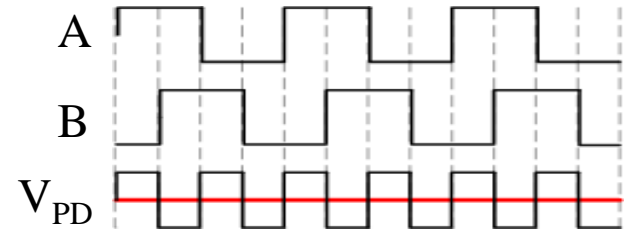
$$\Delta f = 0.05\text{Hz}$$



# Lect. 27: Charge-Pump PLL

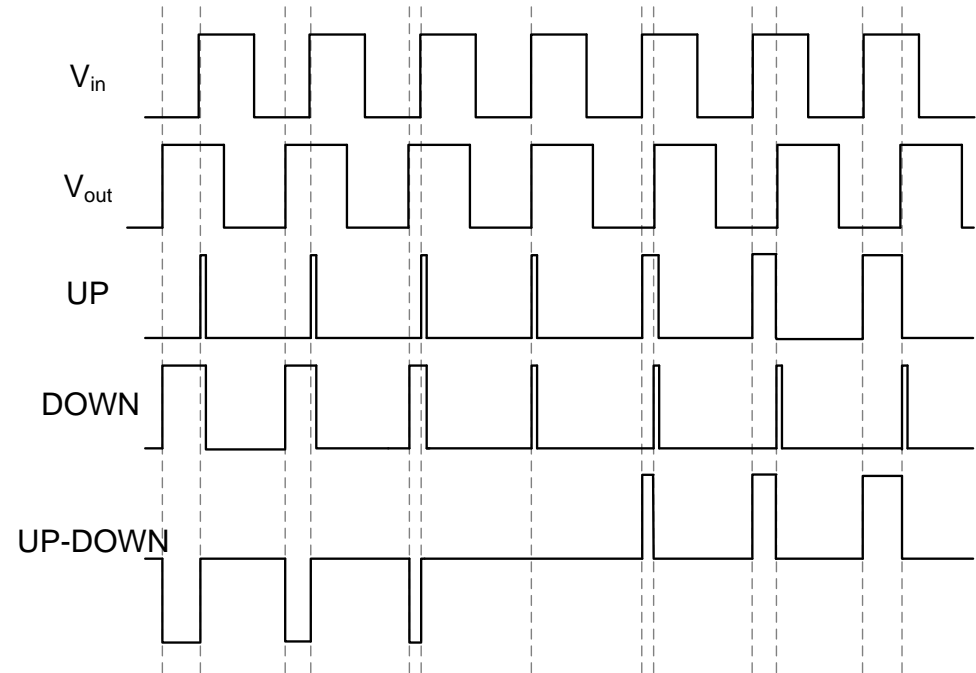
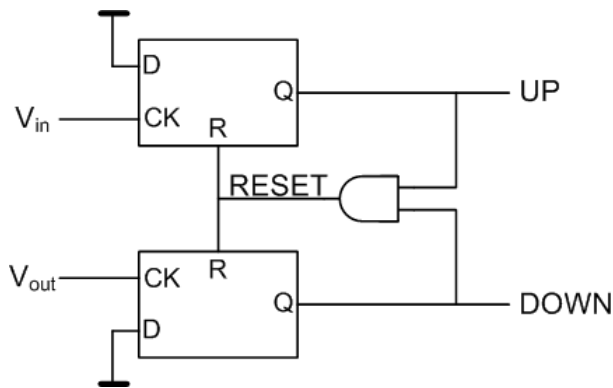
Limitation is due to narrow linear phase detection range

Multiplicier



# Lect. 27: Charge-Pump PLL

Wider range phase detection?

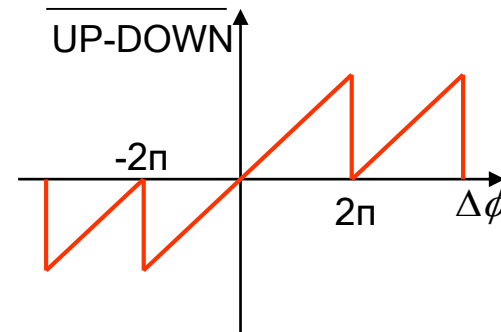


D Flip-flop:

Q becomes D at the rising clock edge

Q resets when R is HIGH

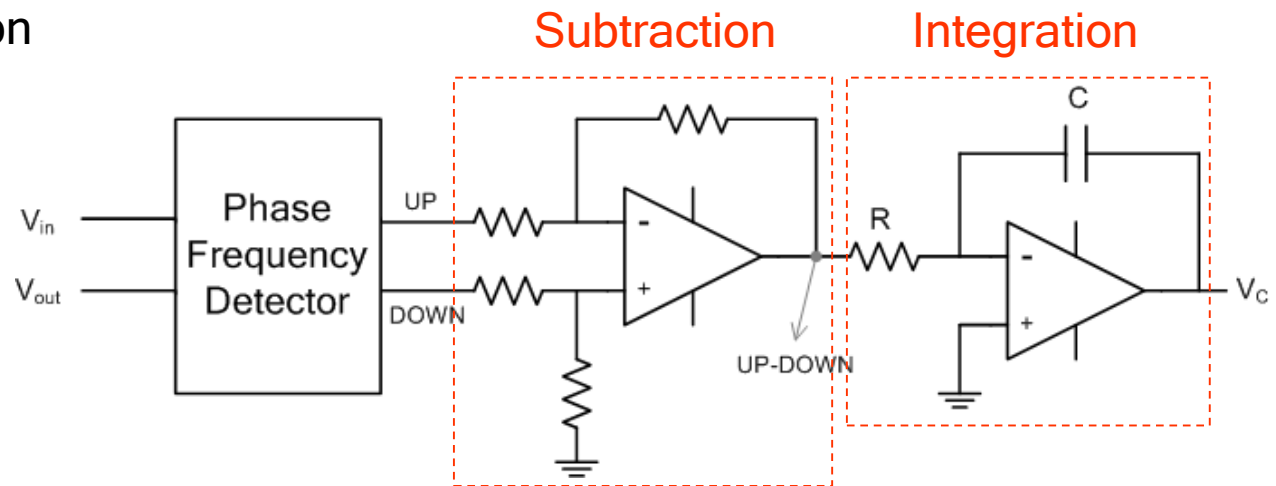
→ Phase and Frequency Detector (PFD)



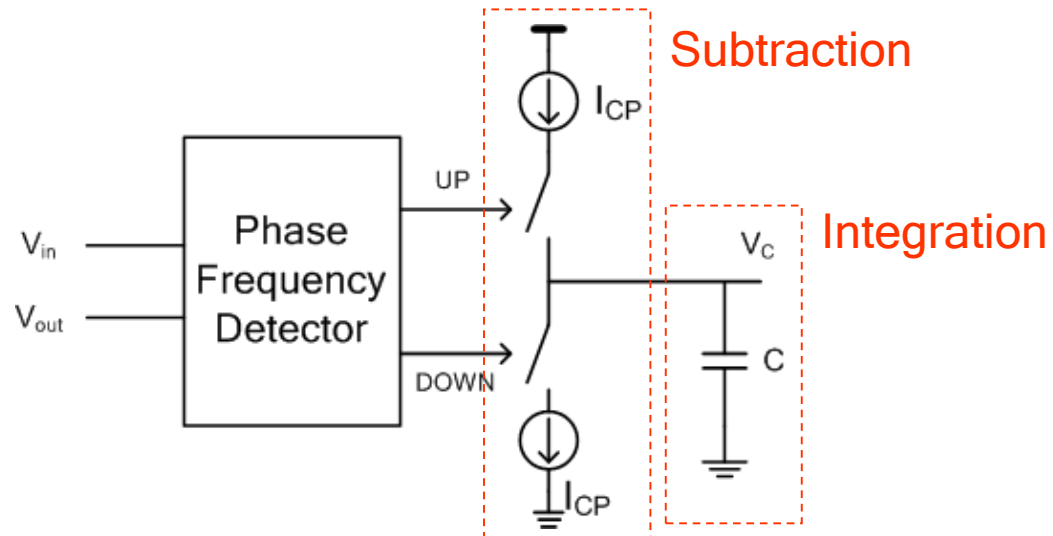
# Lect. 27: Charge-Pump PLL

## Subtraction and integration

Voltage mode  
using OP amplifiers

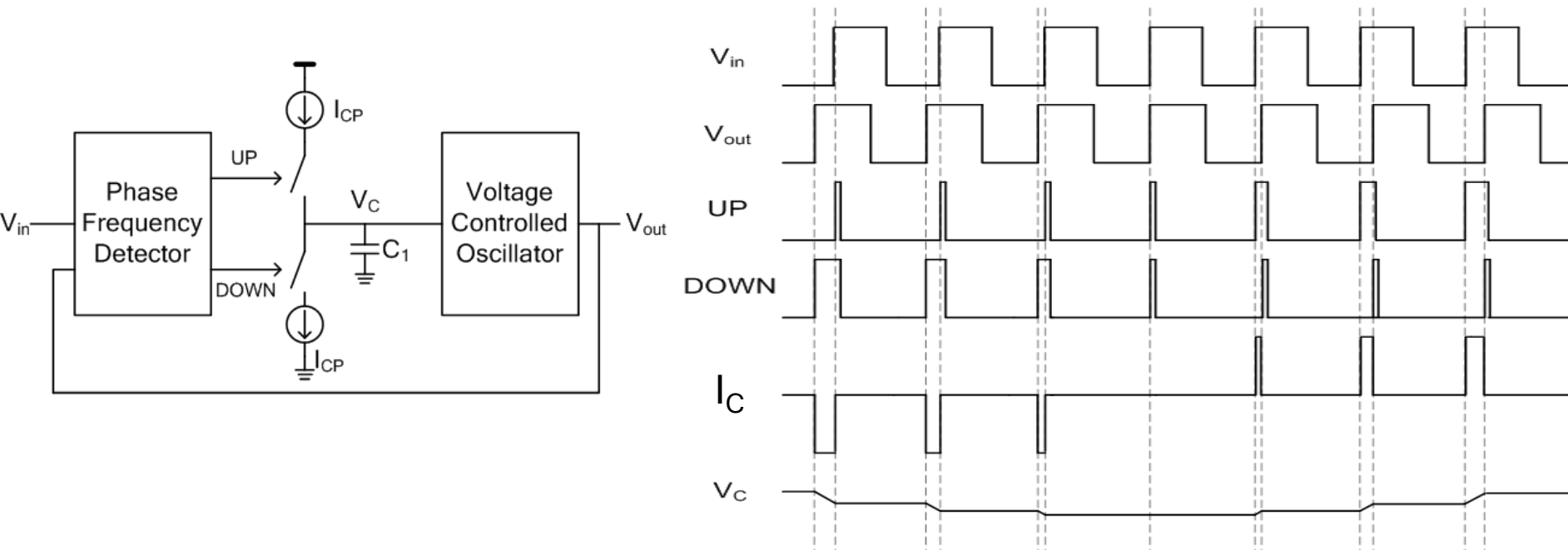


Current mode  
using charge pump

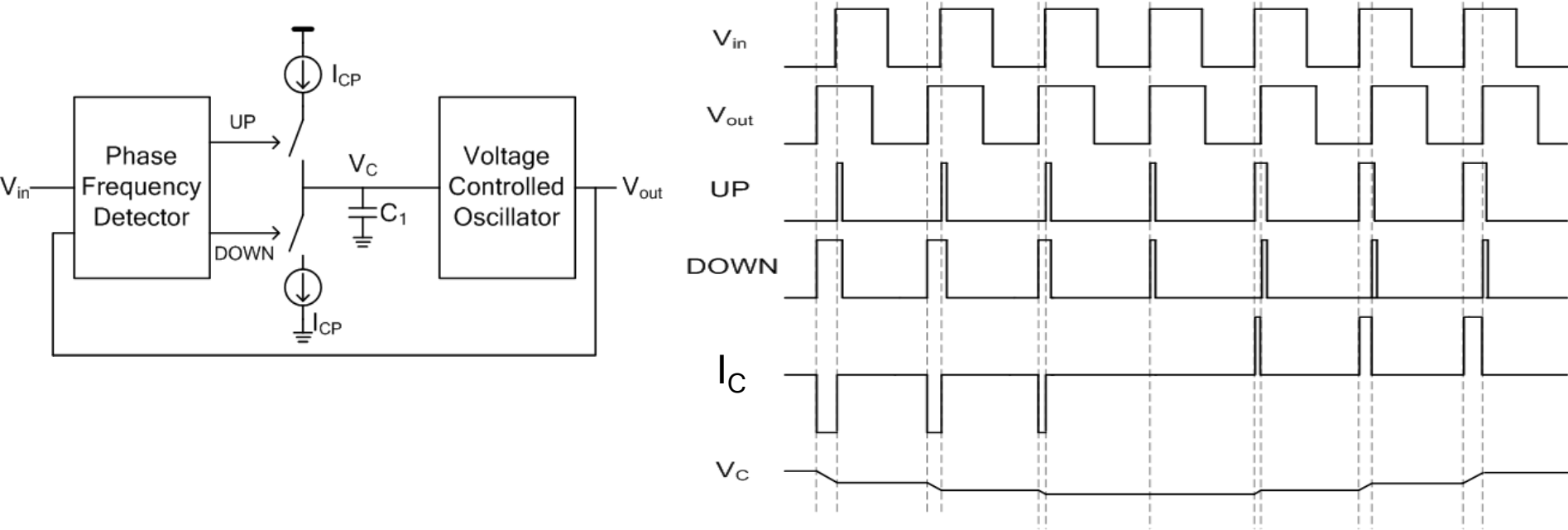


# Lect. 27: Charge-Pump PLL

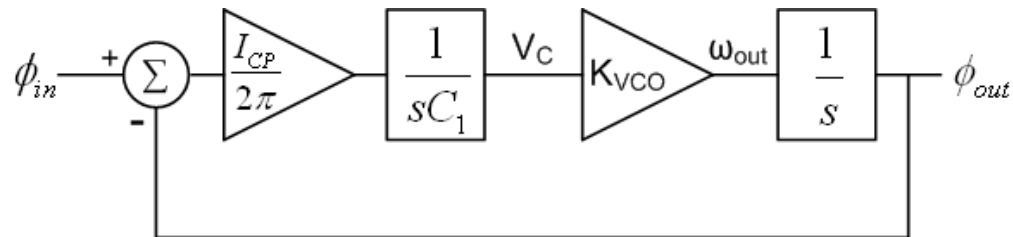
## Charge Pump PLL



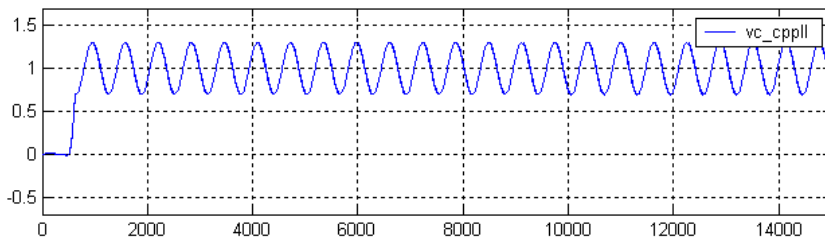
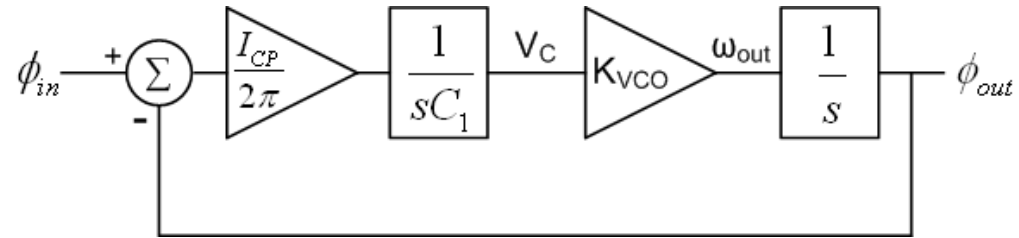
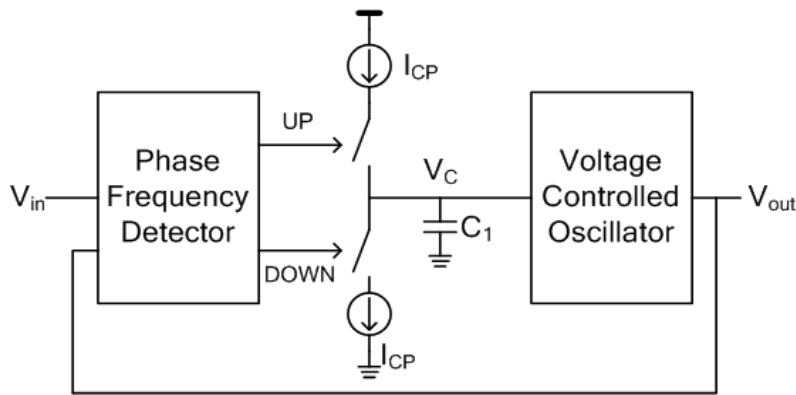
# Lect. 27: Charge-Pump PLL



Linear continuous-time model for charge-pump PLL

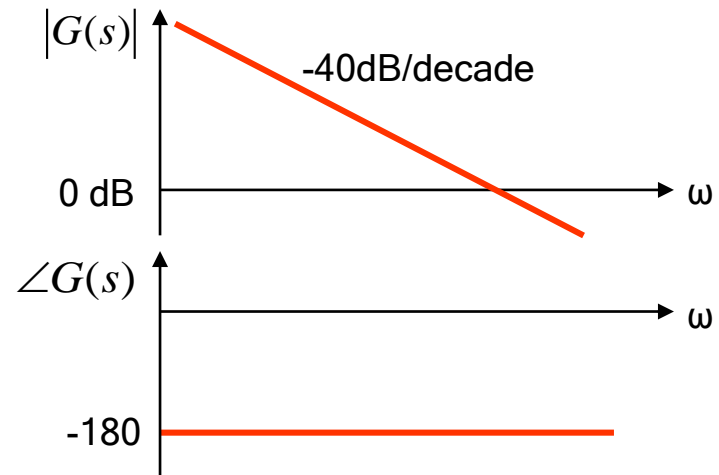


# Lect. 27: Charge-Pump PLL



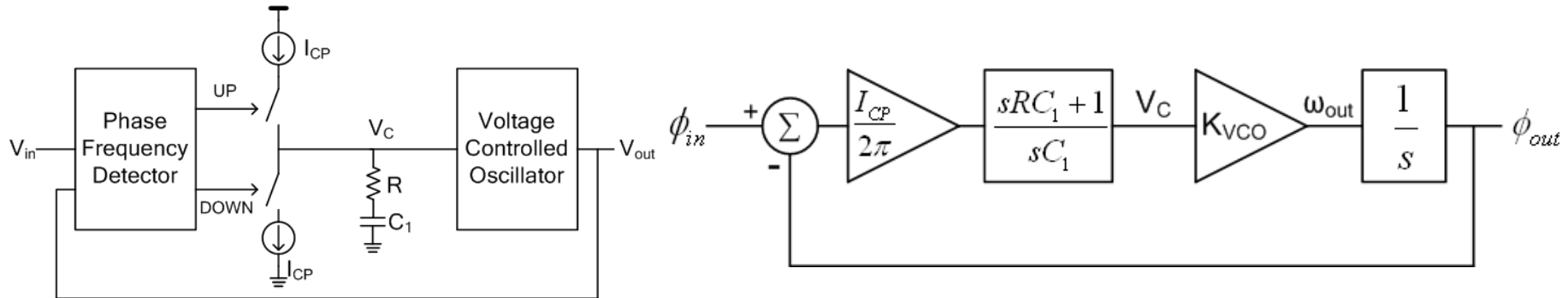
Open loop gain:

$$G(s) = \frac{1}{2\pi} I_{CP} K_{VCO} \frac{1}{s^2 C_1}$$



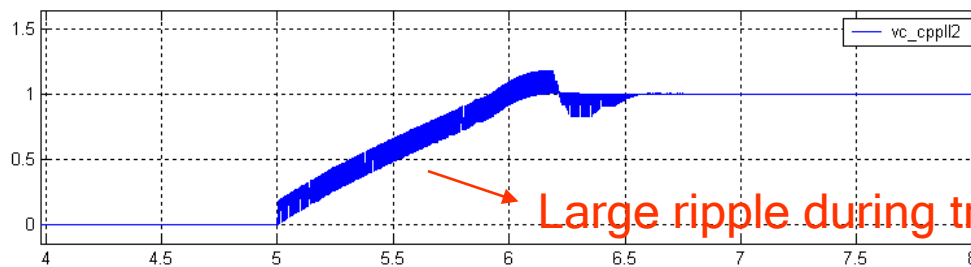
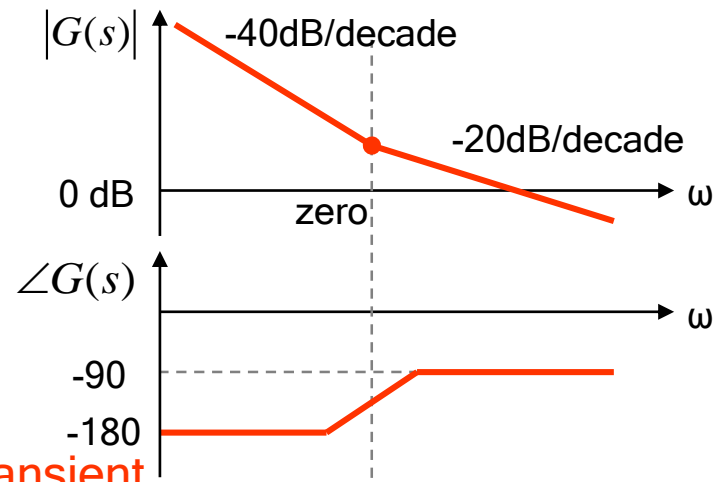
No phase margin  $\rightarrow$  Unstable

# Lect. 27: Charge-Pump PLL



Open loop gain:

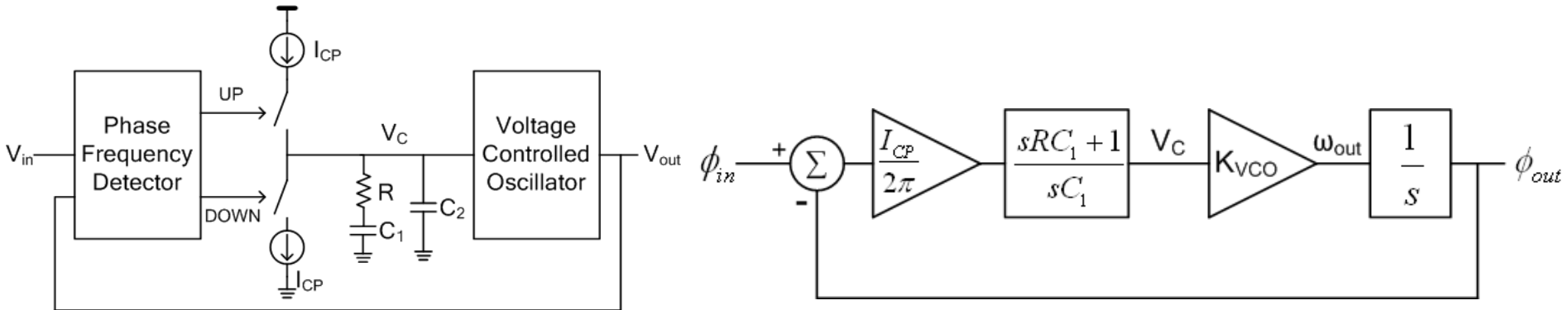
$$G(s) = \frac{1}{2\pi} I_{CP} K_{VCO} \frac{sRC_1 + 1}{s^2 C_1}$$



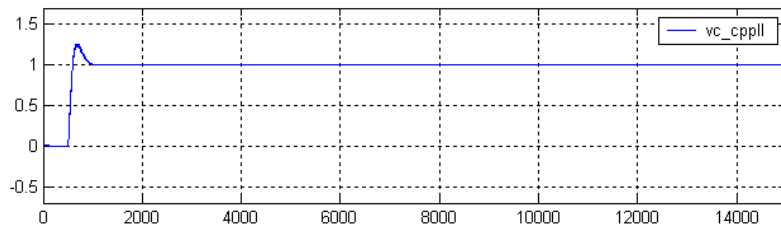


# Lect. 27: Charge-Pump PLL

## Charge Pump PLL



→ Ripple reduction with small  $C_2$  ( $\approx C_1/10$ )



Open loop gain:

Simplification as 2<sup>nd</sup>-order system

$$G(s) \sim \frac{1}{2\pi} I_{CP} K_{VCO} \frac{sRC_1 + 1}{s^2 C_1}$$

# Lect. 27: Charge-Pump PLL

$$G(s) = \frac{1}{2\pi} I_{CP} K_{VCO} \frac{sRC_1 + 1}{s^2 C_1}$$

Closed loop transfer function

$$H(s) = \frac{\frac{I_{CP}}{2\pi C_1} K_{VCO} (RC_1 s + 1)}{s^2 + \frac{I_{CP}}{2\pi} K_{VCO} R s + \frac{I_{CP}}{2\pi C_1} K_{VCO}}$$

$$\omega_0 = \sqrt{\frac{I_{CP} K_{VCO}}{2\pi C_1}} \quad Q = \frac{1}{R \sqrt{I_{CP} C_1 K_{VCO}}}$$

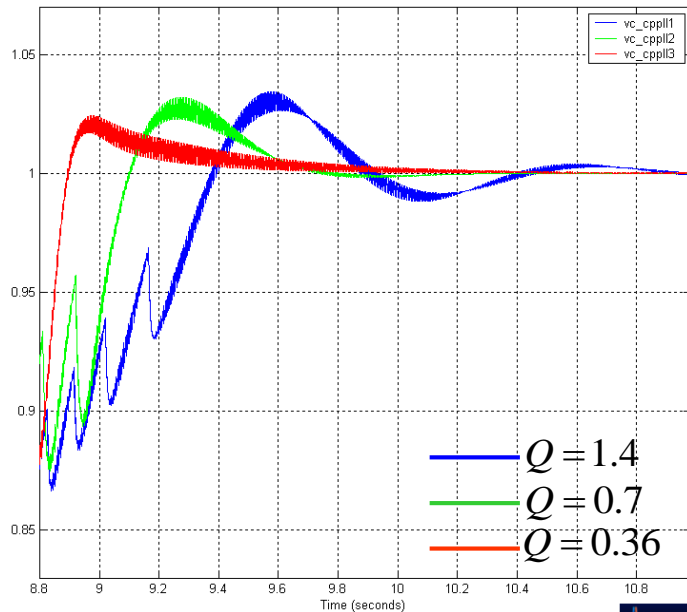
# Lect. 27: Charge-Pump PLL

$$f_{in} = 200\text{Hz}$$

$$I_{CP} = 100\mu\text{A}$$

$$K_{VCO} = 2\pi \times 100\text{rad} / \text{s} / \text{V}$$

$$f_0 = 1\text{Hz}$$



(Q dependence)

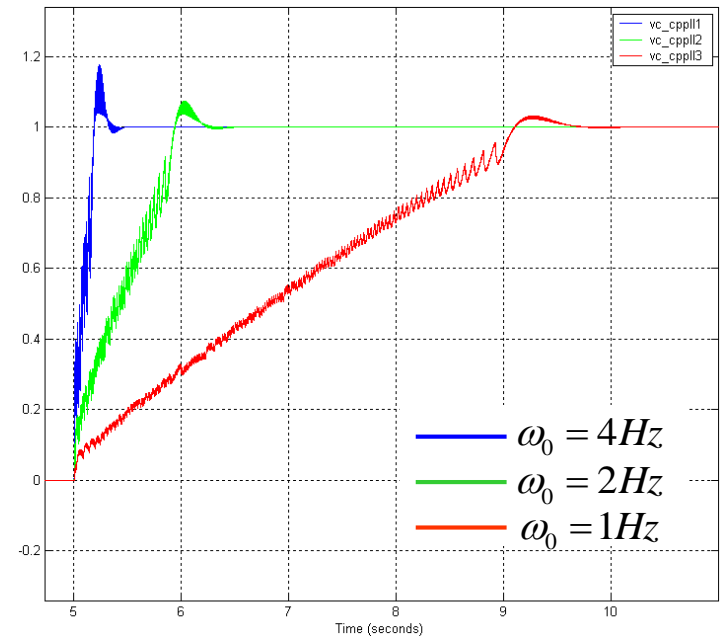
Step response simulations

$$f_{in} = 200\text{Hz}$$

$$I_{CP} = 100\mu\text{A}$$

$$K_{VCO} = 2\pi \times 100\text{rad} / \text{s} / \text{V}$$

$$Q = 0.7$$



( $\omega_0$  dependence)

→ Optimization for desired performance!