

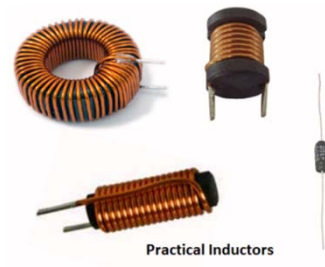
High-Speed Serial Interface Circuits and Systems

Lect. 3 – LC Oscillators

(From Chap. 6 and 7 of Razavi)

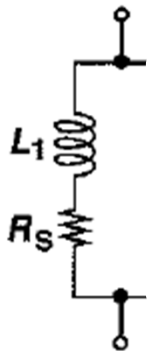
Inductors

- What is an inductor?
- How to make inductors?



$$L = \frac{\mu N^2 A}{l}$$

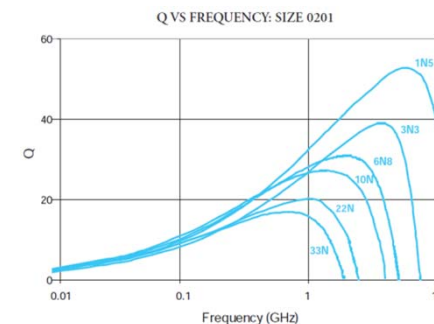
- Non-ideality: Series resistance



Rs:

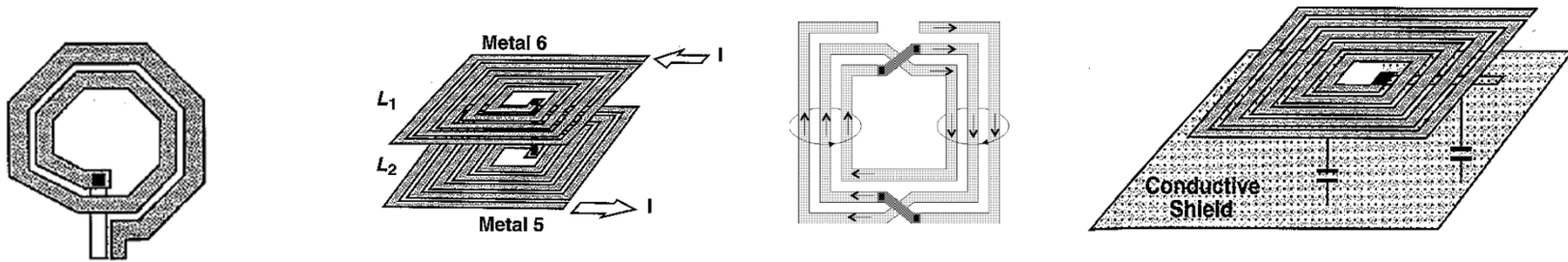
- Finite conductivity
- Skin effect: Surface currents induced by the magnetic field (eddy current) are concentrated near surface and effectively increases the resistance. More pronounced in higher frequency.
- Core loss: Dielectric loss
- Radiation loss

- Quality factor for an inductor: $Q = \omega L/R$ (X/R)
- How does Q change with frequency?



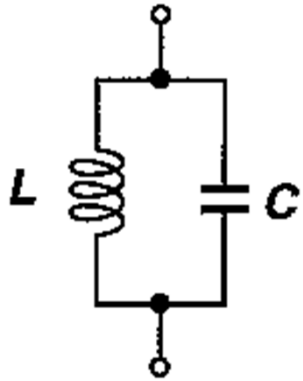
On-Chip Inductors

- How to realize on-chip inductors?



- On-chip inductors are typically lossy and large
- Recently, on-chip inductors are widely used since the required inductance is becoming smaller and processing technology is getting better

LC Tank



In s-domain

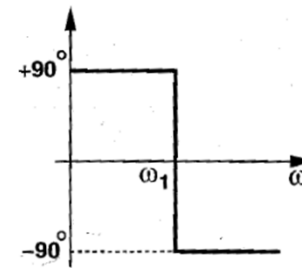
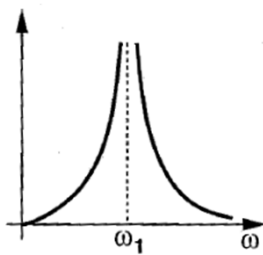
$$Z(s) = sL \parallel \frac{1}{sC} = \frac{sL}{s^2 LC + 1}$$

$$\text{Poles at } s = \pm j \frac{1}{\sqrt{LC}}$$

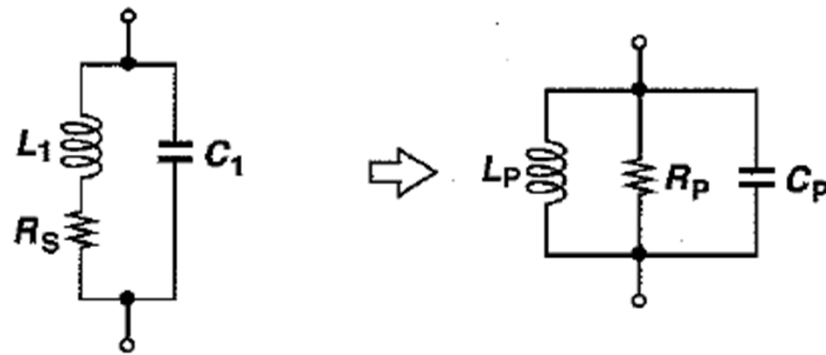
$$\text{In steady-state } s = j\omega \quad Z(j\omega) = \frac{j\omega L}{1 - \omega^2 LC}$$

$$|Z(j\omega)| = \frac{\omega L}{|1 - \omega^2 LC|}$$

$$\angle Z(j\omega) = \frac{\pi}{2} \text{ or } -\frac{\pi}{2}$$



RLC



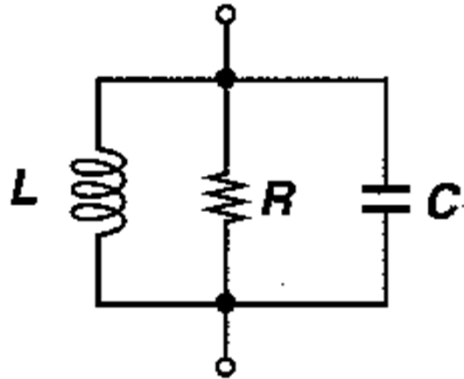
$$C_p = C_1 \quad R_s + L_1 s = R_p L_p s / (R_p + L_p s)$$

$$L_P \approx L_1 \left(1 + \frac{R_S^2}{L_1^2 \omega^2} \right)$$

If $Q (= L_1 \omega / R_s)$ is large $L_P \approx L_1$

$$R_p \sim L_1^2 \omega^2 / R_s \sim Q^2 R_s$$

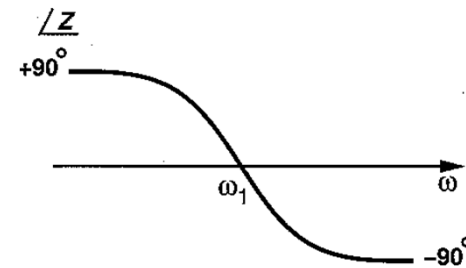
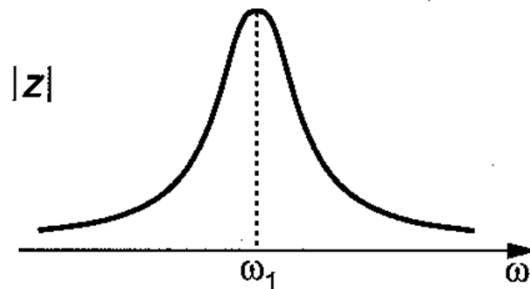
RLC



$$Z(s) = sL \parallel \frac{1}{sC} \parallel R = \frac{RLs}{RLCs^2 + Ls + R} = \frac{s/C}{s^2 + \frac{1}{RC}s + \frac{1}{LC}}$$

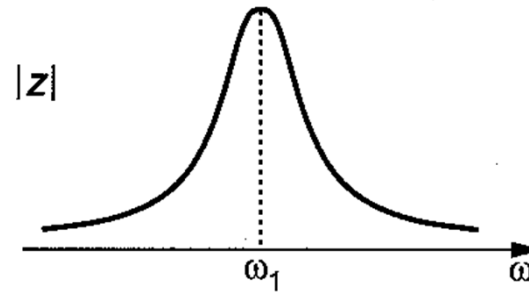
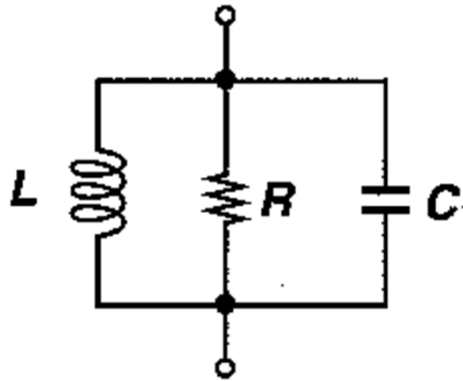
Poles at $s = \frac{-\frac{1}{RC} \pm \sqrt{\left(\frac{1}{RC}\right)^2 - \frac{4}{LC}}}{2}$

Two complex conjugate poles if $\left(\frac{1}{RC}\right)^2 < \frac{4}{LC} \rightarrow \text{Under-damping}$



Magnitude peak and zero phase at $\omega = \frac{1}{\sqrt{LC}}$

RLC



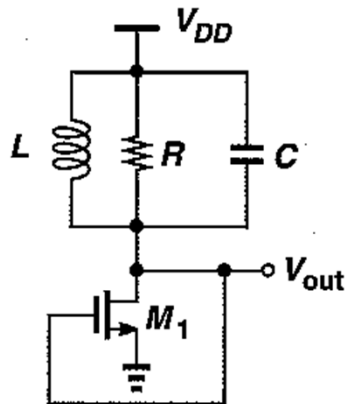
Q-factor: $2\pi \times (\text{Energy Stored} / \text{Energy dissipated per cycle})$

$$Q = R\sqrt{\frac{C}{L}}$$

For large Q, 3-dB bandwidth: $\frac{1}{\sqrt{LCQ}}$

LC Oscillator

Oscillation?

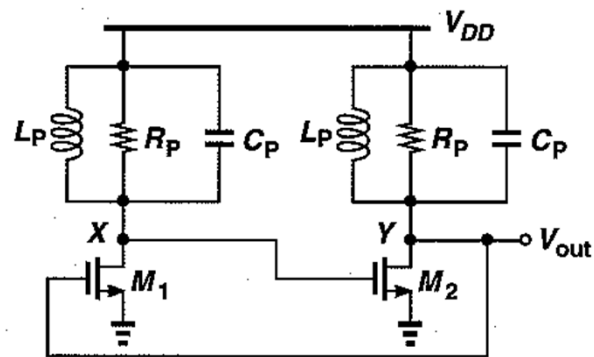


Assume M_1 has no capacitive component

At low frequency

At high frequency

At resonance frequency

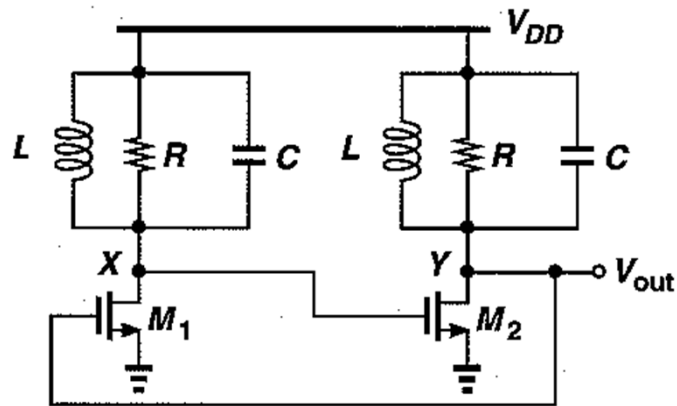


Oscillation!

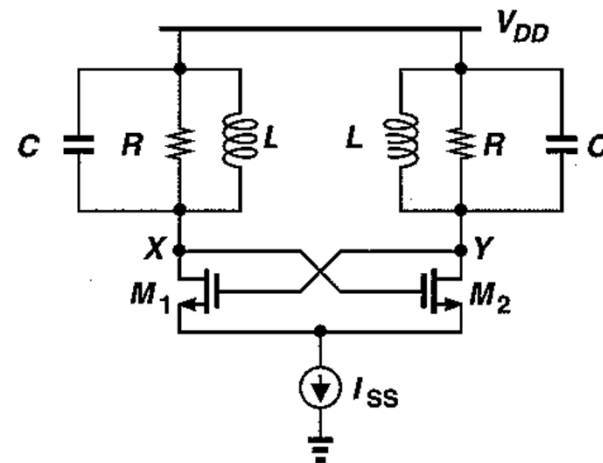
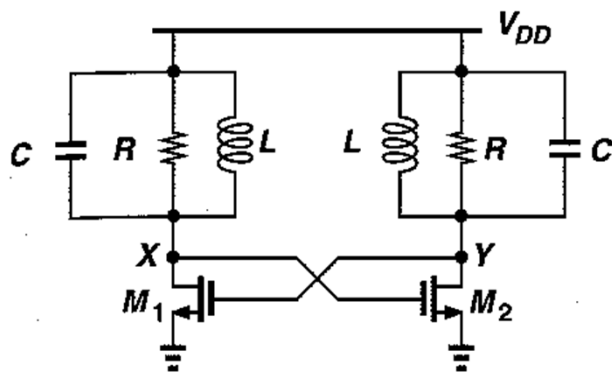
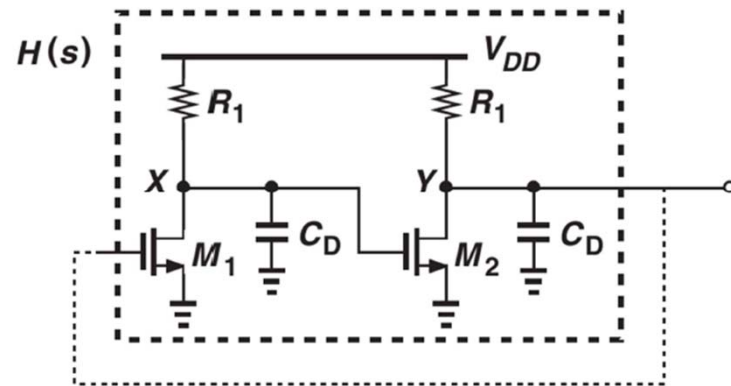
$$\omega = \frac{1}{\sqrt{LC}}$$

$$g_m R_p = 1$$

Cross-Coupled LC Oscillator



VS

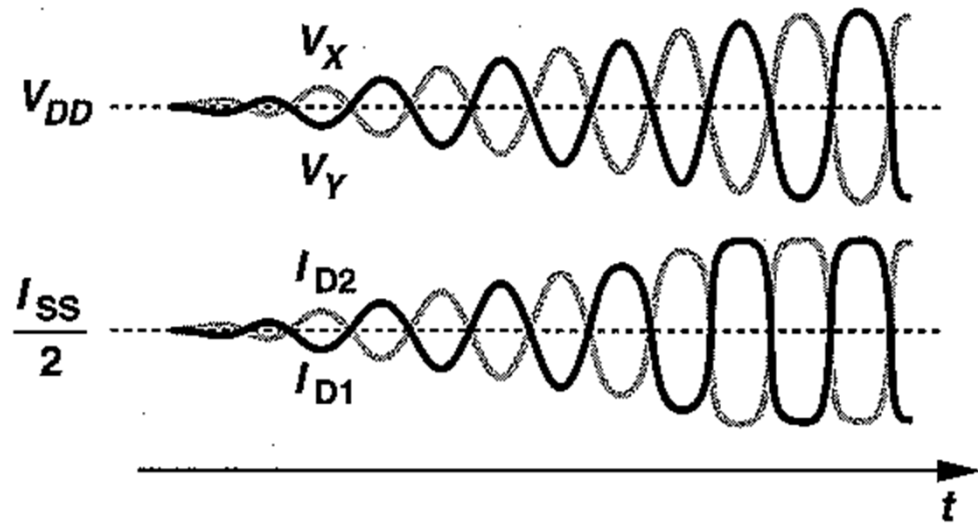
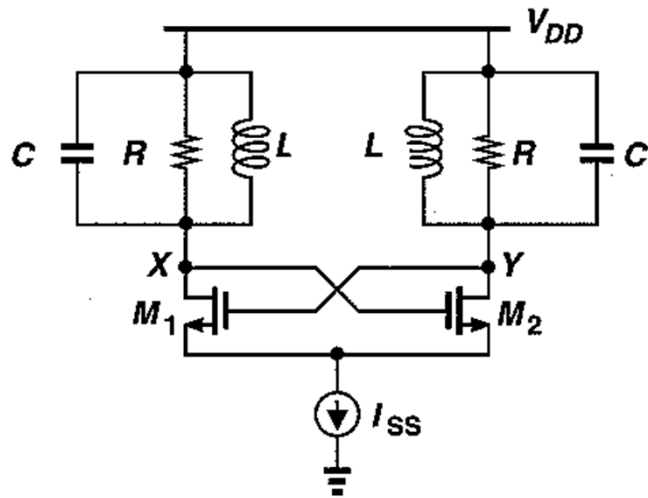


→ Cross-Coupled LC Oscillator

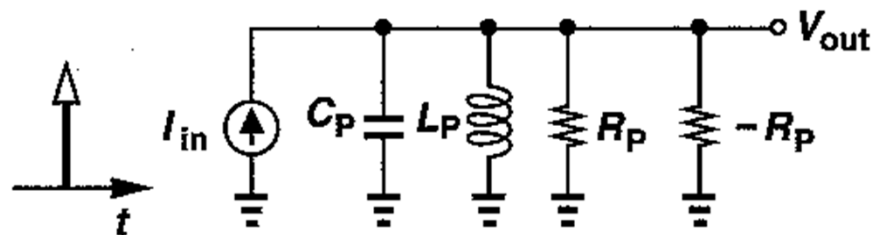
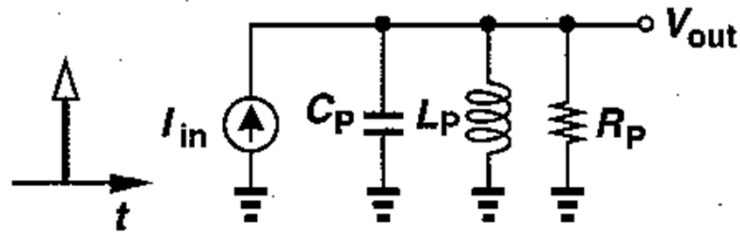
Cross-Coupled LC Oscillator

What initiates oscillation?

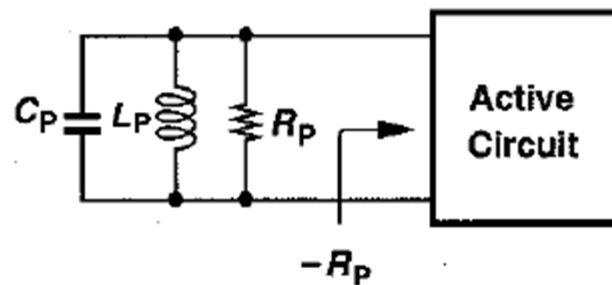
What limits oscillation?



Negative G_m Oscillator

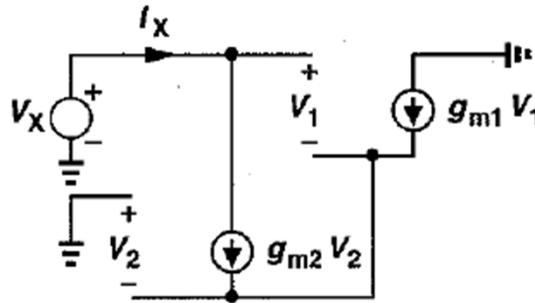
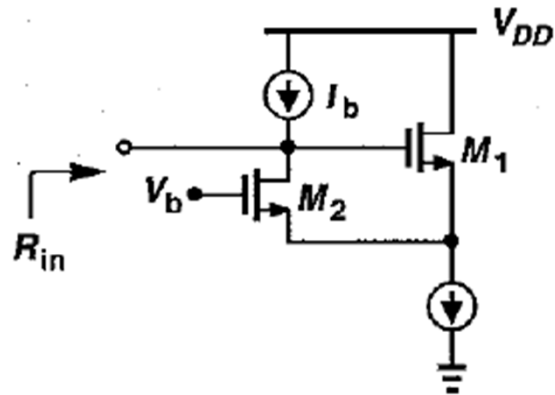


How do you make negative resistance circuit?



Active circuit with negative resistance in small signal

Negative Resistance Circuits

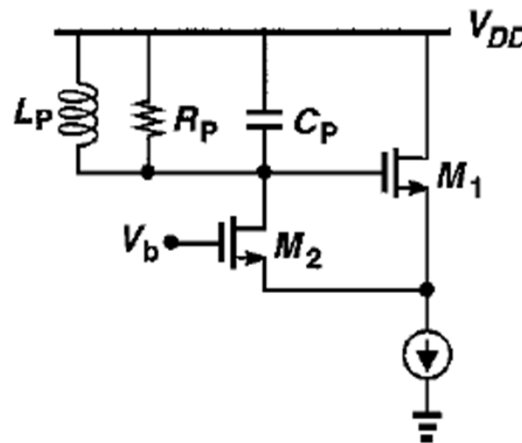
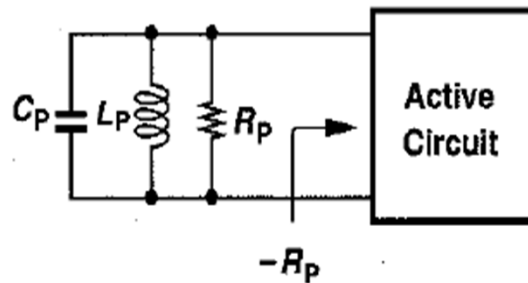


$$V_X = V_1 - V_2$$

$$I_X = g_{m2}V_2 = -g_{m1}V_1$$

$$V_X = -\frac{I_X}{g_{m1}} - \frac{I_X}{g_{m2}}$$

$$R_{in} = \frac{V_X}{I_X} = -\frac{1}{g_{m1}} - \frac{1}{g_{m2}}$$



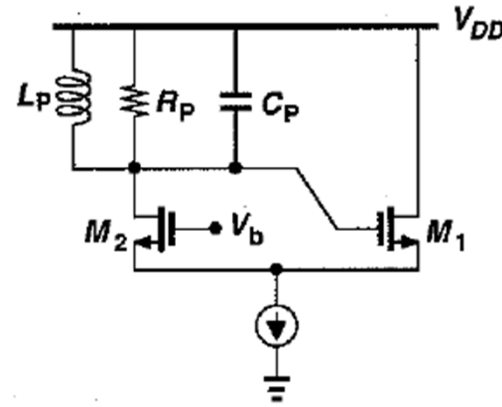
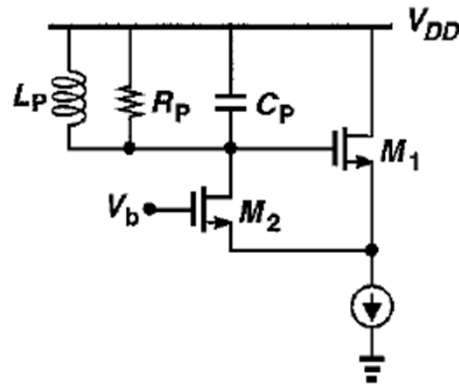
Negative G_m oscillator

Oscillation frequency?

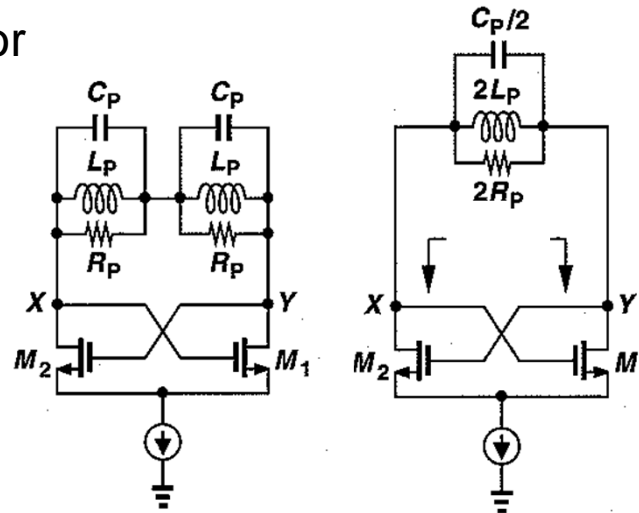
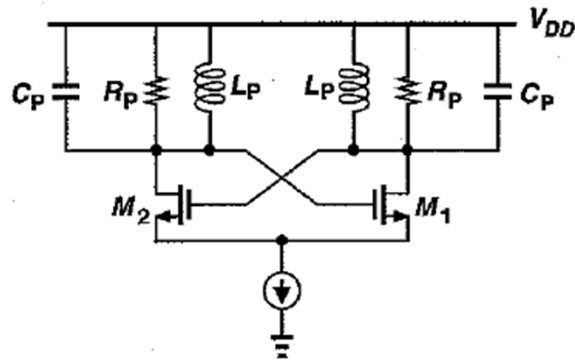
Oscillation condition?

$$R_p = \frac{2}{g_m}$$

Negative- G_m Oscillator



Differential Negative- G_m Oscillator



$$R_{in} = -\frac{1}{g_{m1}} - \frac{1}{g_{m2}}$$

$$2R_p = \frac{2}{g_m}$$

Same configuration as cross-coupled LC oscillator

$$g_m R_p = 1$$

Negative- G_m Oscillator

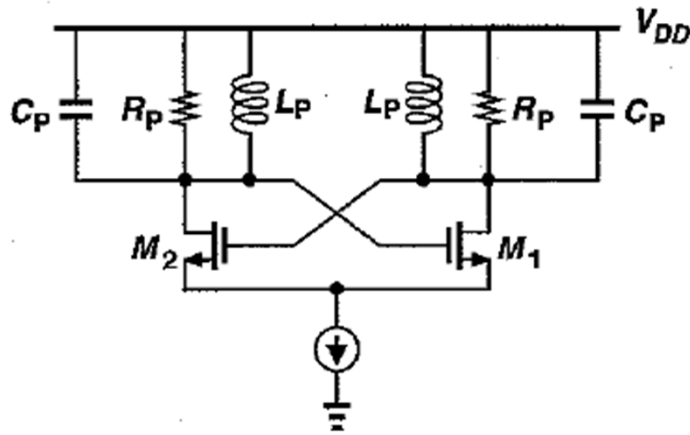
There many different types of oscillator circuits.

Sometimes your circuit oscillates when you do not want it.
(unwanted feedback)

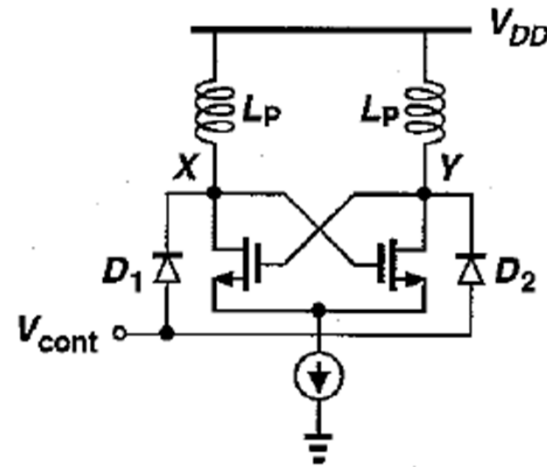
LC vs ring oscillators?

- LC provides cleaner oscillation (Smaller phase noise)
- RO is easier to implement for CMOS IC
- For very high-frequency applications, LC are used

Voltage-Controlled LC Oscillator



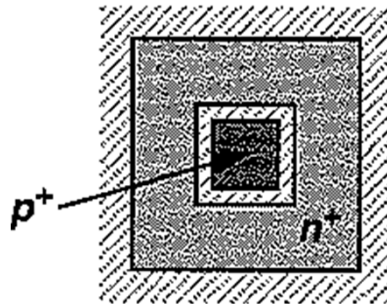
Easiest to tune C_p with varactors



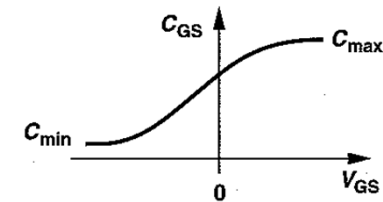
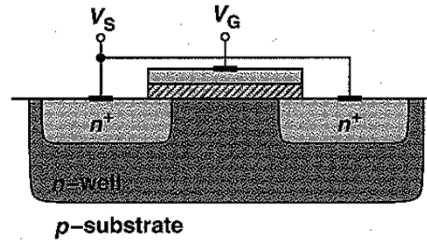
R_p is usually due to parasitic resistance for the inductor

Varactors

Reverse biased PN junction



Accumulation MOS Varactor

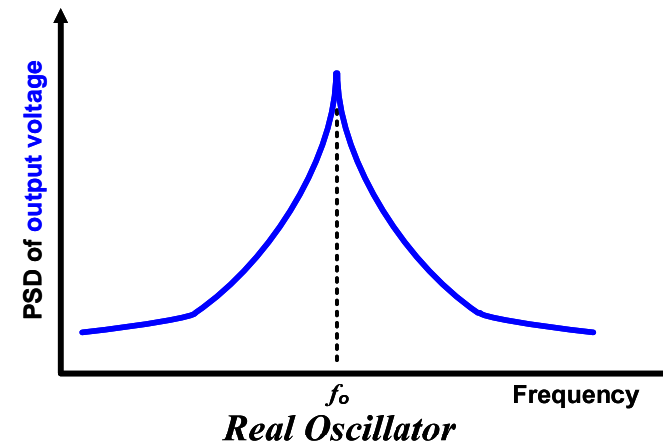
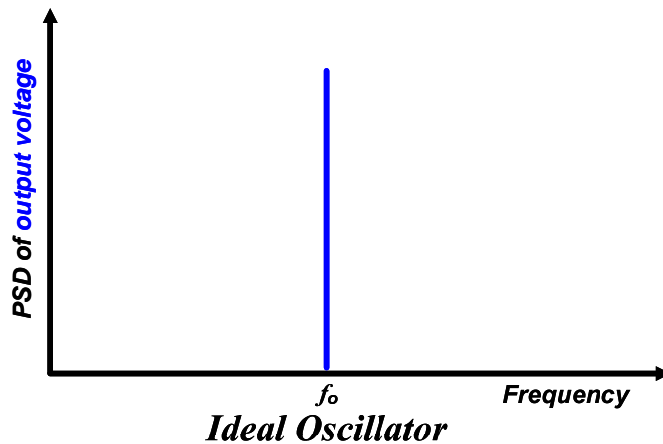


$$C_{var} = \frac{C_0}{\left(1 + \frac{V_R}{\phi_B}\right)^m}$$

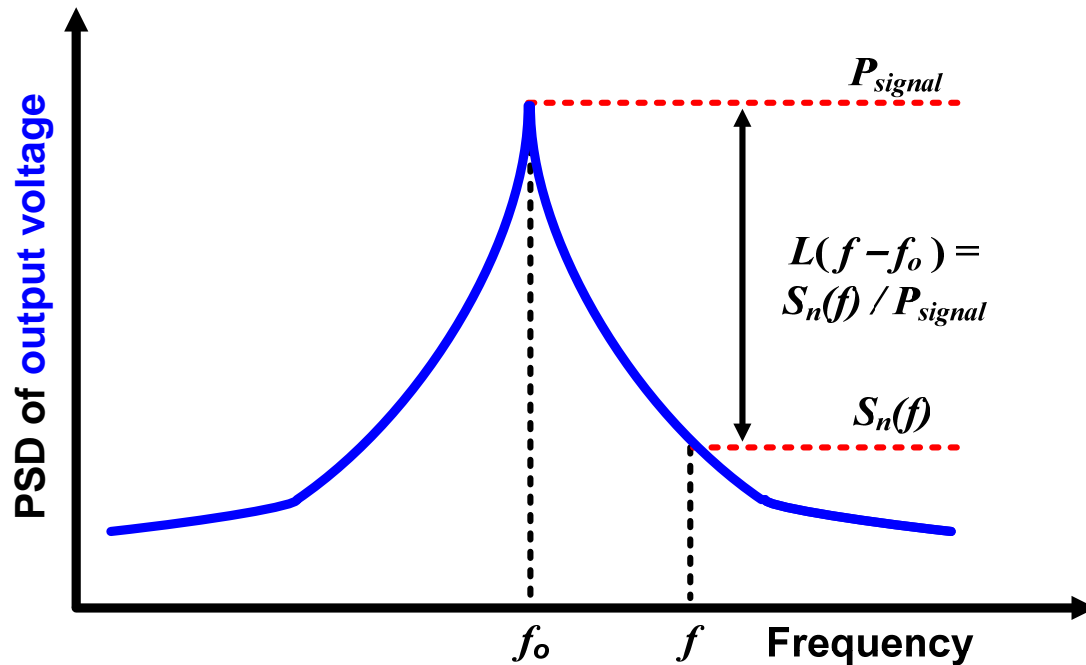
Tuning range is limited
Very nonlinear

Phase Noise

- Ideal oscillator vs Real oscillator



Phase Noise



- Phase noise represented as single sideband noise (SSN) in log(dB) scale.

$$L(\omega) = 10 \log \frac{S_n(\omega - \omega_o, \omega - \omega_o)}{P_{signal}(\omega_o)} \text{ (dBc / Hz)} \sim \frac{4kT}{P_{dissipation}} \left(\frac{\omega_o}{2Q\omega} \right)^2$$

Design Exercise

