

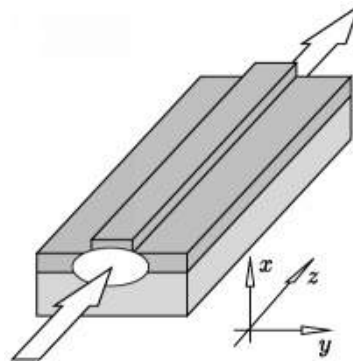
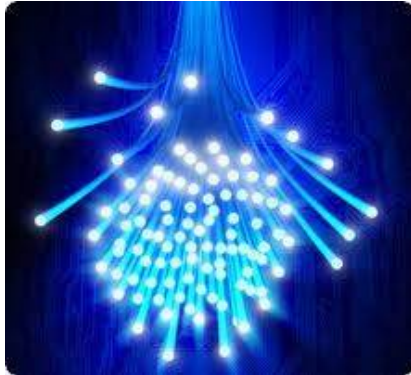
Opto-Electronics and Photonics

Lecture 18 : Planar Waveguide Devices

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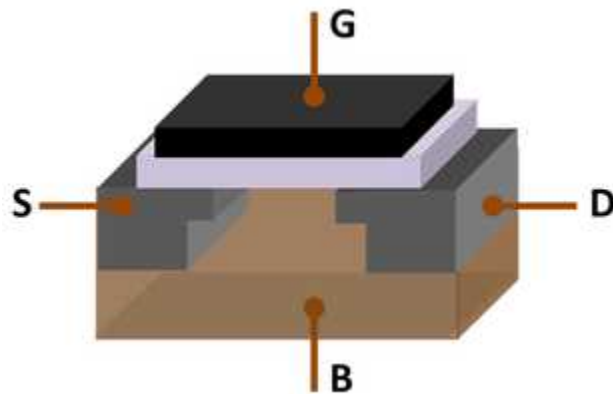
Lecture 18: Planar Waveguide Devices



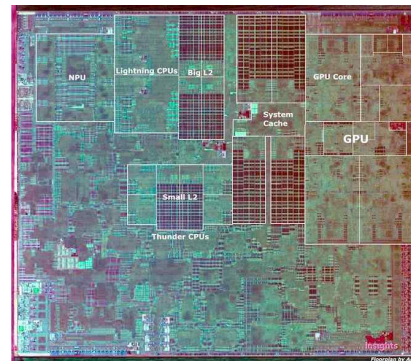
Planar waveguide

➔ Device

➔ Photonic Integrated Circuit



Transistor

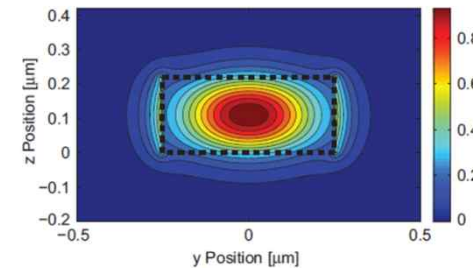
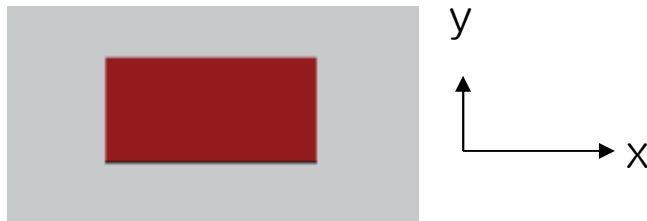


Integrated Circuit

Lecture 18: Planar Waveguide Devices

3-Dimensional waveguide

→ Numerical solution easily available



Detailed analysis complicated

Intensity profile for the fundamental TE mode

In general, TE_{mn} TM_{mn} modes

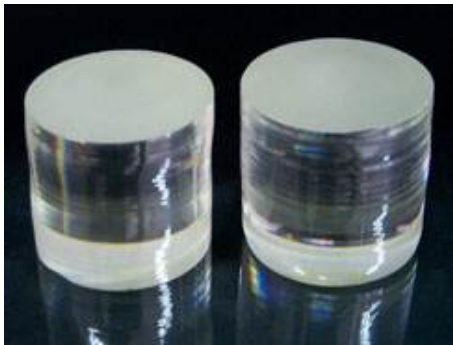
Materials requirements for planar dielectric waveguides

- Precise control of dimension and refractive index
- Low loss at desired λ
- Mass production possible
- Electrical control of refractive index (Electro-optic effect)
- Integration

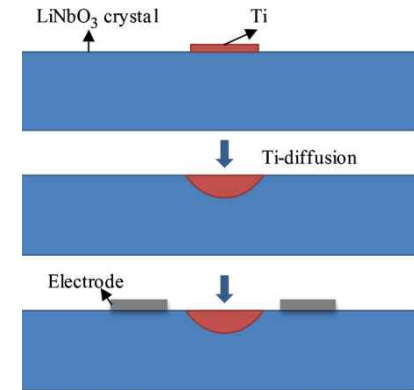
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Materials used for waveguides

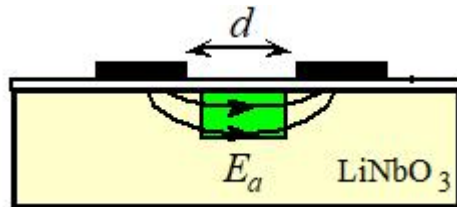
- Ceramics : LiNbO_3 (Lithium Niobate) with Ti doping for core



Transparent to $1.55\mu\text{m}$ light



Efficient refractive index modulation by E-field
(Large electro-optic effect)

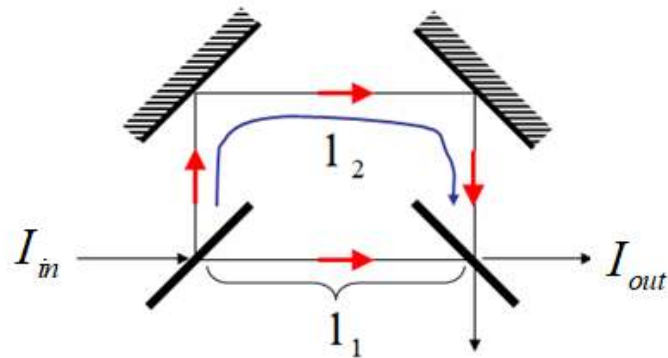


$$\Delta n_{eff} \sim E$$

- Phase modulation of incident light
- Mach-Zehnder Modulator

Lecture 18: Planar Waveguide Devices

Mach-Zehnder Interferometer (Lecture 12)

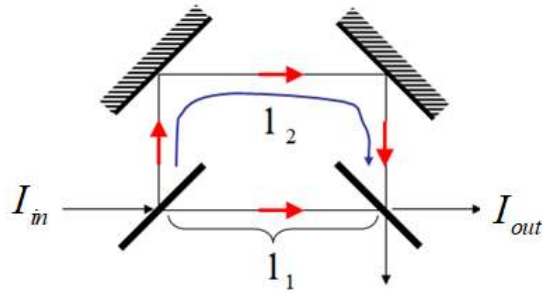


$$\frac{I_{out}}{I_{in}} = \cos^2\left(\frac{kl_1 - kl_2}{2}\right)$$

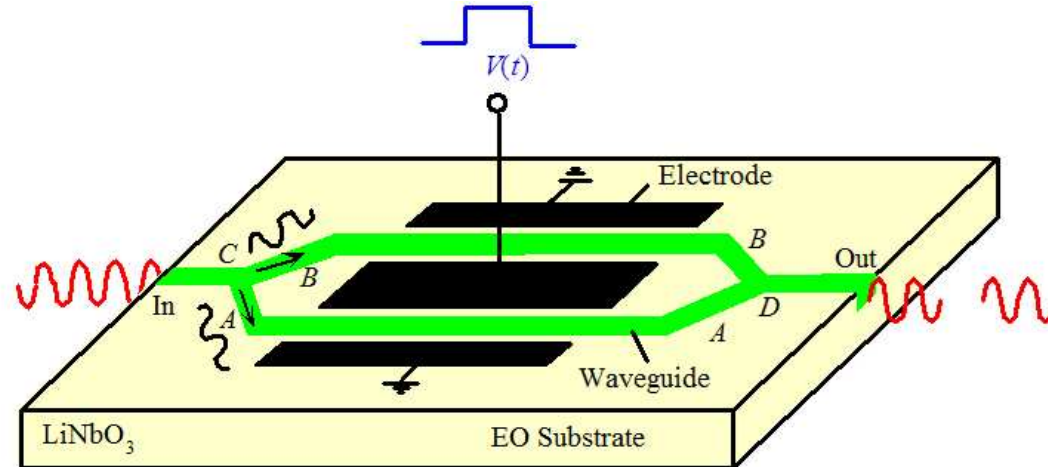
If $(kl_1 - kl_2)$ can be changed with voltage, I_{out} can be modulated

→ Optical intensity modulator

Lecture 18: Planar Waveguide Devices



$$\frac{I_{out}}{I_{in}} = \cos^2\left(\frac{kl_1 - kl_2}{2}\right)$$



Upper arm: $n_{eff} + \Delta n_{eff}(V)$

Lower arm: $n_{eff} - \Delta n(V)$

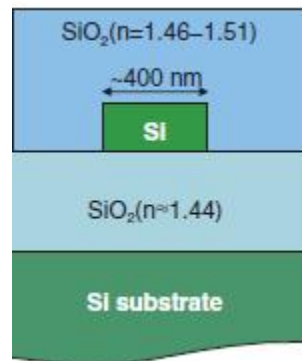
$$\frac{I_{out}}{I_{in}} = \cos^2\left(\frac{kl_1 - kl_2}{2}\right) \rightarrow \cos^2\left(\frac{(n_{eff} + \Delta n_{eff})k_0l - (n_{eff} - \Delta n_{eff})k_0l}{2}\right) = \cos^2(\Delta n_{eff}k_0l)$$

Mach-Zehnder Modulator (MZM) => A key device for high-speed optical comm.

But not good for mass production, integration

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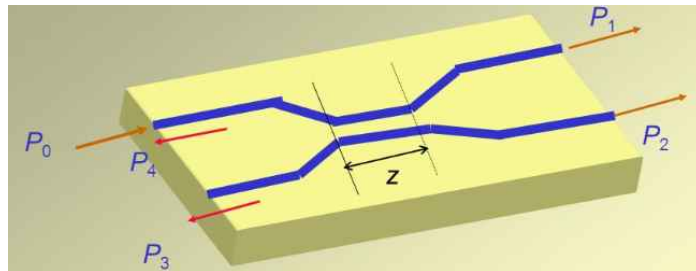
Sol (Si on Insulator) Si (core)/ SiO₂ (cladding)



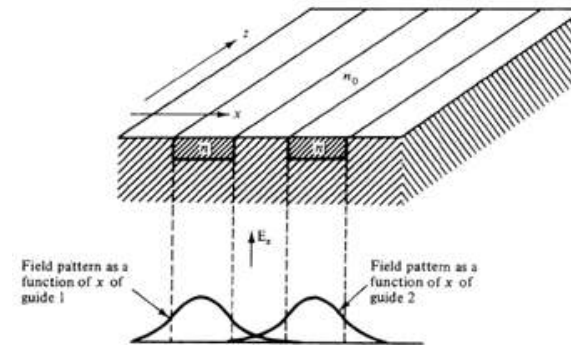
- Si is transparent to 1.55 μ m light → Good planar waveguides
- Not efficient E-O effect
- Si fabrication technology very mature → Advanced technique for Si intensity modulators
- Si Photonic Integrated Circuits

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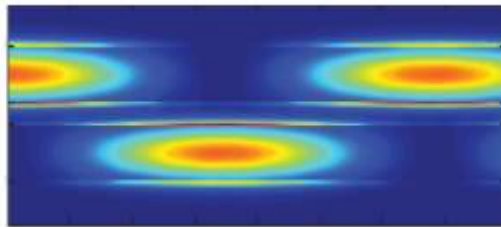
- Directional Coupler



Two waveguides placed very close to each other



Energy transfer between two waveguides



$$P_1 = P_0 \cos^2(az)$$

$$P_2 = P_0 \sin^2(az)$$

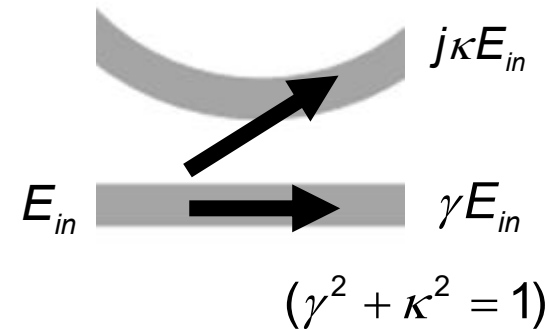
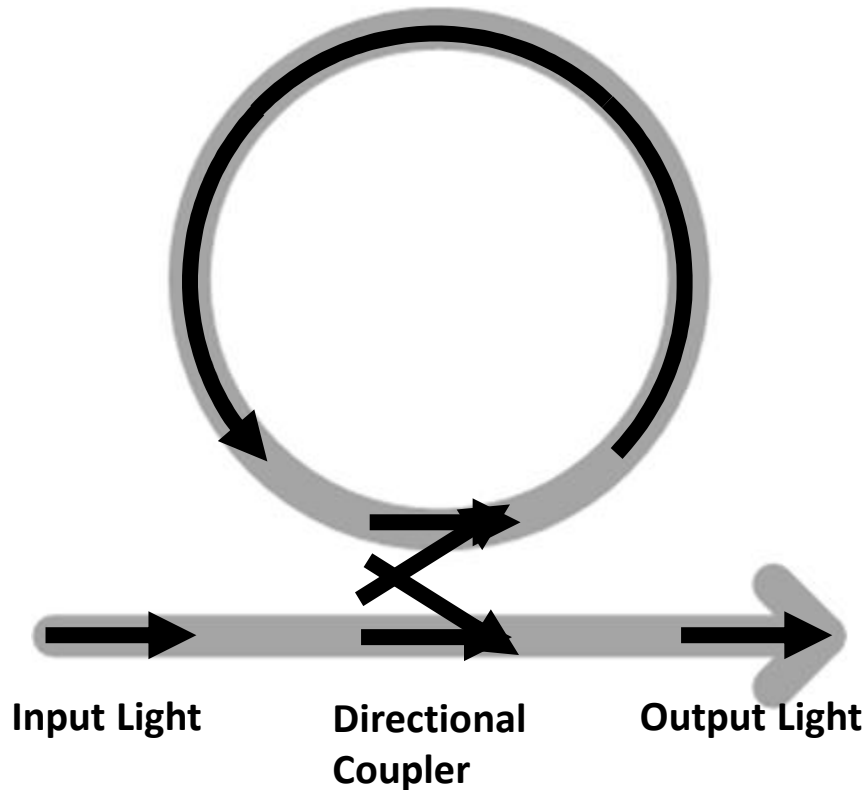
$az = \pi/2 \rightarrow$ Spatial switch

$az = \pi/4 \rightarrow$ Power divider (Beam Splitter)

Amount of coupling can be changed by carrier injection or temperature

Lecture 18: Planar Waveguide Devices

- Ring Resonator (Top View)



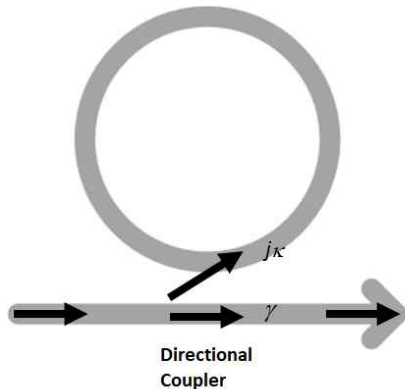
α : amount after one circulation

L : ring circumference

$$E_{out} = E_{in}\gamma + E_{in}(j\kappa)(\alpha e^{-jn_{eff}k_0L})(j\kappa) + E_{in}(j\kappa)(\alpha e^{-jn_{eff}k_0L})\gamma(\alpha e^{-jn_{eff}k_0L})(j\kappa) \dots$$

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- Ring Resonator (Top View)

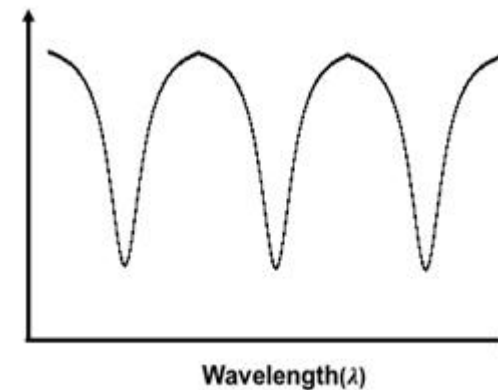


$$(\theta = n_{eff} k_0 L)$$

$$\frac{E_{out}}{E_{in}} = \gamma - \kappa^2 \alpha e^{-j\theta} - \kappa^2 \alpha^2 \gamma e^{-j2\theta} - \kappa^2 \alpha^3 \gamma^2 e^{-j3\theta} - \dots$$

$$= \gamma - \kappa^2 \sum_{n=1}^{\infty} \alpha^n \gamma^{n-1} e^{-jn\theta} = \gamma - \frac{\kappa^2 \alpha e^{-j\theta}}{1 - \alpha \gamma e^{-j\theta}} = \frac{\gamma - \alpha e^{-j\theta}}{1 - \alpha \gamma e^{-j\theta}}$$

$$E_{out} = E_{in} \gamma + E_{in} (j\kappa) (\alpha e^{-jn_{eff} k_0 L}) (j\kappa) \\ + E_{in} (j\kappa) (\alpha e^{-jn_{eff} k_0 L}) \gamma (\alpha e^{-jn_{eff} k_0 L}) (j\kappa) \\ \dots$$

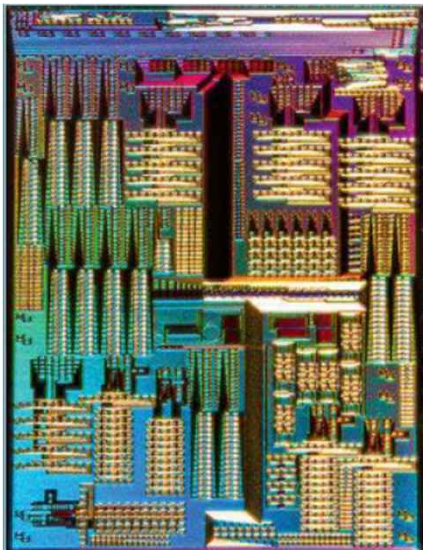


Interferometer ←

It can be shown min. transmission occurs when $\theta = 2m\pi \implies L = m \frac{\lambda_{res}}{n_{eff}}$

Lecture 18: Planar Waveguide Devices

Si Photonic Integrated Circuits Si PIC's used in High-Performance Data Centers



Lecture 18: Planar Waveguide Devices

Homework (Due 11/15)

Consider a Mach-Zehnder interferometer shown below. The effective index that $1.5\ \mu\text{m}$ light experiences while traveling inside the interferometer is 3.5 when no bias voltage is applied. Due to manufacturing problems, $l_1 = 100\ \mu\text{m}$ and $l_2 = 100.1\ \mu\text{m}$ are not the same.

(a) What is the output power when the input power is 1mW at $1.5\ \mu\text{m}$ and no bias is applied? Assume P_{out} has \cos^2 dependence on P_{in} .

We want to use the interferometer as an optical on/off switch by applying voltage to the upper arm as shown. The effective index of the upper arm increases 0.001 per 1 volt applied.

(b) What is the voltage with the smallest absolute value that needs to be applied to make the switch on?

